NEW JERSEY DEPT OF ENVIRONMENTAL PROTECTION TRENTON F/G 13/13 NATIONAL DAM SAFETY PROGRAM, LAKE INTERVALE DAM (NJ00769), PASS--ETC(U) AD-A101 533 MAY 81 R J MCDERMOTT, J E GRIBBIN DACW61-79-C-0011
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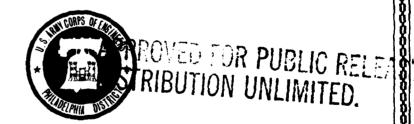
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PASSAIC RIVER BASIN, TROY BROOK, MORRIS COUNTY

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PHASE 1. INSPECTION REPORT. NATIONAL DAM SAFETY PROGRAM



THE DEPARTMENT OF ARMY

> Philadelphia District Corps of Engineers Philadelphia, Pennsylvania REPT. NO: DAEN[MAP-53842/ NJ 00769-81/05

> > MAY 1981

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National Dam Safety Program. Lake Intervale Dam (NJ00769), Passaic River Basin, Troy Brook, Morris County,

SIFICATION OF THIS PAGE New Jersey. Phase I Inspection Reports REPORT DOCUMENTATION PAGE BEFORE COMPLETING FORM 2. GOVT ACCESSION NO. 3. RECIPIENT'S CATALOG NUMBER DD-A10153E DAEN/NAP**#**53842/NJ**0**0769-81/**6**5 TITLE (and Subtitle) S. TYPE OF REPORT & PERIOD COVERED Phase I Inspection Report FINAL Y 1 National Dam Safety Program PERFORMING ORG. REPORT NUMBER Lake Intervale Dam J00769 Morris County, NJ McDermot, Richard J., P.B. M. D. .. 8. CONTRACT OR GRANT NUMBER(+) DACW61-79-C-0011 Gribbin, John E., P.E. 10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS 9. PERFORMING ORGANIZATION NAME AND ADDRESS Storch Engineers 220 Ridgedale Ave. Florham Park, N.J. 07932 12. REPORT DATE 1. CONTROLLING OFFICE NAME AND ADDRESS NJ Department of Environmental Protection Division of Water Resources May**⊊ 1**981 13. NUMBER OF PAGES P.O. Box CNO29 Trenton, NJ 08625 4. MONITORING AGENCY NAME & ADDRESS(II different from Controlling Office) 18. SECURITY CLASS. (of this report) U.S. Army Engineer District, Philadelphia Custom House, 2d & Chestnut Streets Unclassified Philadelphia, PA 19106 18a, DECLASSIFICATION/DOWNGRADING 16. DISTRIBUTION STATEMENT (of thie Report) Approved for public release; distribution unlimited. 17. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, If different from Report) 18. SUPPLEMENTARY NOTES Copies are obtainable from National Technical Information Service, Springfield, Virginia 22151. 19. KEY WORDS (Continue on reverse side if necessary and identify by block number) Dams National Dam Safety Program Embankments Lake Intervale Dam, NJ Vigual Inspection Spillways Structural Analysis Erosion ABSTRACT (Continue on reverse side if necessary and identify by block number) This report cites results of a technical investigation as to the dam's adequacy. The inspection and evaluation of the dam is as prescribed by the National Dam Inspection Act, Public Law 92-367. The technical investigation includes visual inspection, review of available design and construction records, and preliminary structural and hydraulic and hydrologic calculations, as applicable. An assessment of the dam's general condition is included in the report.

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## DEPARTMENT OF THE ARMY PHILADELPHIA DISTRICT. CORPS OF ENGINEERS CUSTOM HOUSE-2D & CHESTNUT STREETS PHILADELPHIA, PENNSYLVANIA 19106

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Honorable Brendan T. Byrne Governor of New Jersey Trenton, New Jersey 08621

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Dear Governor Byrne:

Inclosed is the Phase I Inspection Report for Lake Intervale Dam in Morris County, New Jersey which has been prepared under authorization of the Dam Inspection Act, Public Law 92-367. A brief assessment of the dam's condition is given in the front of the report.

Based on visual inspection, available records, calculations and past operational performance, Lake Intervale Dam, initially listed as a high hazard potential structure, but reduced to a significant hazard potential structure as a result of this inspection, is judged to be in good overall condition. The dam's spillway is considered inadequate because a flow equivalent to ten percent of the One Hundred Year Flood would cause the dam to be overtopped. To ensure adequacy of the structure, the following actions, as a minimum, are recommended:

- a. The spillway's adequacy should be determined by a qualified professional consultant engaged by the owner using more sophisticated methods, procedures and studies within six months from the date of approval of this report. Within three months of the consultant's findings remedial measures to ensure spillway adequacy should be initiated.
- b. Within six months from the date of approval of this report the following remedial actions should be initiated:
- (1) Trees and adverse vegetation on the dam embankment should be removed.
- (2) The eroded area on the downstream side of the embankment should be properly filled and stabilized.
- c. When the water level returns to its normal level, the dam and its appurtenances should be inspected for seepage.
- d. The owner should develop written operating procedures and a periodic maintenance plan to ensure the safety of the dam, within one year from the date of approval of this report.

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NAPEN-N Honorable Brendan T. Byrne

e. An emergency action plan and warning system should be developed which outlines actions to be taken by the owner to minimize the downstream effects of an emergency at the dam within six months from the date of approval of this report.

A copy of the report is being furnished to Mr. Dirk C. Hofman, New Jersey Department of Environmental Protection, the designated State Office contact for this program. Within five days of the date of this letter, a copy will also be sent to Congressman Courter of the Thirteenth District. Under the provision of the Freedom of Information Act, the inspection report will be subject to release by this office, upon request, five days after the date of this letter.

Additional copies of this report may be obtained from the National Technical Information Services (NTIS), Springfield, Virginia 22161 at a reasonable cost. Please allow four to six weeks from the date of this letter for NTIS to have copies of the report available.

An important aspect of the Dam Inspection Program will be the implementation of the recommendations made as a result of the inspection. We accordingly request that we be advised of proposed actions taken by the State to implement our recommendations.

Sincerely,

l Incl As stated JAMES G. TON
Colonel, Corps of Engineers
Commander and District Engineer

Copies furnished:

Mr. Dirk C. Hofman, P.E., Deputy Director Division of Water Resources N.J. Dept. of Environmental Protection P.O. Box CNO29 Trenton, NJ 08625

Mr. John O'Dowd, Acting Chief Bureau of Flood Plain Regulation Division of Water Resources N.J. Dept. of Environmental Protection P.O. Box CN029 Trenton, NJ 08625

#### LAKE INTERVALE DAM (NJ00769)

#### CORPS OF ENGINEERS ASSESSMENT OF GENERAL CONDITIONS

This dam was inspected on 18 December 1980 by Storch Engineers, under contract to the State of New Jersey. The State, under agreement with the U.S. Army Engineer District, Philadelphia, had this inspection performed in accordance with the National Dam Inspection Act, Public Law 92~367.

Lake Intervale Dam, initially listed as a high hazard potential structure, but reduced to a significant hazard potential structure as a result of this inspection, is judged to be in good overall condition. The dam's spillway is considered inadequate because a flow equivalent to ten percent of the One Hundred Year Flood would cause the dam to be overtopped. To ensure adequacy of the structure, the following actions, as a minimum, are recommended:

- a. The spillway's adequacy should be determined by a qualified professional consultant engaged by the owner using more sophisticated methods, procedures and studies within six months from the date of approval of this report. Within three months of the consultant's findings remedial measures to ensure spillway adequacy should be initiated.
- b. Within six months from the date of approval of this report the following remedial actions should be initiated:
- (1) Trees and adverse vegetation on the dam embankment should be removed.
- (2) The eroded area on the downstream side of the embankment should be properly filled and stabilized.
- c. When the water level returns to its normal level, the dam and its appurtenances should be inspected for seepage.
- d. The owner should develop written operating procedures and a periodic maintenance plan to ensure the safety of the dam, within one year from the date of approval of this report.
- e. An emergency action plan and warning system should be developed which outlines actions to be taken by the owner to minimize the downstream effects of an emergency at the dam within six months from the date of approval of this report.

APPROVED:

JAMES G. TON

Colonel, Corps of Engineers

Commander and District Engineer

DATE:

AIE:

### PHASE I REPORT NATIONAL DAM SAFETY PROGRAM

Name of Dam:

Lake Intervale Dam, I.D. NJ00769

State Located:

New Jersey

County Located:

Morris

Drainage Basin:

Passaic River

Stream:

Troy Brook

Date of Inspection:

December 18, 1980

#### Assessment of General Condition of Dam

Based on visual inspection, past operational performance and Phase I engineering analyses, Lake Intervale Dam is assessed as being in good overall condition.

Based on investigations of the downstream flood plain made in connection with this report, it is recommended that the hazard potential classification be downgraded from high to significant hazard.

Hydraulic and hydrologic analyses indicate that the spillway is inadequate. Discharge from the spillway is not sufficient to pass the designated spillway design flood (100-year storm) without an overtopping of the dam. The spillway is capable of passing approximately 9 percent of the SDF. Therefore, the owner should engage a professional engineer experienced in the design and construction of dams in the near future to perform more accurate hydraulic and hydrologic analyses relating to spillway capacity. Based on the findings of the analyses, the need for, and the type of remedial measures should be determined and then implemented.

The owner should, in the near future, develop an emergency action plan together with an effective warning system outlining actions to be taken by the operator to minimize downstream effects of an emergency at the dam.

Also, when the water level returns to its normal level, the dam and its appurtenances should be inspected for seepage. (Lake water level was drawn down at the time of inspection.)

In addition, it is recommended that the following remedial measures be undertaken by the owner in the near future.

- 1) Trees and adverse vegetation on the dam embankment should be removed.
- 2) The eroded area on the downstream side of the embankment should be properly filled and stabilized.

In the future, the owner of the dam should develop written operating procedures and a periodic maintenance plan to ensure the safety of the dam.

Richard J. McDermott, P.E.

John E. Gribbin, P.E.



OVERVIEW - LAKE INTERVALE DAM 20 JANUARY 1981

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#### **PREFACE**

This report is prepared under guidance contained in the Recommended Guidelines for Safety Inspection of Dams, for Phase I Investigations. Copies of these guidelines may be obtained from the Office of Chief of Engineers, Washington, D.C. 20314. The purpose of a Phase I Investigation is to identify expeditiously those dams which may pose hazards to human life or property. The assessment of the general condition of the dam is based upon available data and visual inspections. Detailed investigation, and analyses involving topographic mapping, subsurface investigations, testing, and detailed computational evaluations are beyond the scope of a Phase I investigation; however, the investigation is intended to identify any need for such studies.

In reviewing this report, it should be realized that the reported condition of the dam is based on observations of field conditions at the time of inspection along with data available to the inspection team. It is important to note that the condition of dam depends on numerous and constantly changing internal and external conditions, and is evolutionary in nature. It would be incorrect to assume that the present condition of the dam will continue to represent the condition of the dam at some point in the future. Only through continued care and inspection can there be any chance that the unsafe conditions be detected.

Phase I inspections are not intended to provide detailed hydraulic and hydrologic analyses. In accordance with the established Guidelines, the Spillway Test flood is based on the estimated "Probable Maximum Flood" for the region (greatest reasonably possible storm runoff), or fractions thereof. The test flood provides a measure of relative spillway capacity and serves as an aid in determining the need for more detailed hydraulic and hydrologic studies, considering the size of the dam, its general condition and the downstream damage potential.

PHASE I INSPECTION REPORT

NATIONAL DAM SAFETY PROGRAM

LAKE INTERVALE DAM, I.D. NJ00769

SECTION 1: PROJECT INFORMATION

#### 1.1 General

a. Public Law 92-367, August 8, 1972, authorized the Secretary of the Army, through the Corps of Engineers, to initiate a National Program of Dam Inspection throughout the United States. The Division of Water Resources of the New Jersey Department of Environmental Protection (NJDEP) in cooperation with the Philadelphia District of the Corps of Engineers has been assigned the responsibility of supervising the inspection of dams within the State of New Jersey. Storch Engineers has been retained by the NJDEP to inspect and report on a selected group of these dams. The NJDEP is under agreement with the Philadelphia District of the Corps of Engineers.

#### b. Purpose of Inspection

The visual inspection of Lake Intervale Dam was made on December 18, 1980. The purpose of the inspection was to make a general assessment of the structural integrity and operational adequacy of the dam structure and its appurtenances.

#### 1.2 <u>Description of Project</u>

#### a. Description

The dam is an earth embankment with a concrete spillway structure fitted with a timber stoplog. A concrete core wall extends along the embankment for a portion of its length and a timber bridge spans the spillway structure.

The outlet works consist of a gated 12" transite pipe which transversely penetrates the dam embankment to the left of the spillway. The outlet discharges into the downstream channel at a point approximately 50 feet downstream of the dam.

The crest and downstream face of the dam is stabilized by grass while the upstream face is covered with grass and brush. The left portion of the embankment, for a distance of about 400 feet, consists of a paved parking area.

The elevation of the spillway crest is 378.0 National Geodetic Vertical Datum (N.G.V.D.) while that of the crest of dam is 380.9. The elevation of the invert of the outlet works is 373.5 while that of the channel bed at the spillway is 374.7. The overall length of the dam is 520 feet and its height is 6.2 feet.

#### b. Location

Lake Intervale Dam is located in the Township of Parsippany-Troy Hills, Morris County, New Jersey. It impounds a recreational lake known as Lake Intervale, adjacent to Lake Drive which provides principal access. Discharge from the spillway of the dam flows into a branch of the Troy Brook.

#### c. Size and Hazard Classification

The dam is classified in accordance with criteria presented in "Recommended Guidelines for Safety Inspection of Dams" published by the U.S. Army Corps of Engineers. Size categories consist of Small, Intermediate and Large while hazard categories are designated as Low, Significant and High.

<u>Size Classification:</u> Lake Intervale Dam is classified as "Small" size since its maximum storage volume is 89 acre-feet (which is less than 1000 acre-feet) and its height is 6.2 feet (which is less than 40 feet).

Hazard Classification: Visual inspection of the downstream flood plain of the dam together with breach analysis indicate that failure of the dam due to overtopping would not cause inundation of the dwellings downstream from the dam. Failure due to overtopping could result in damage to the road bridge located 150 feet from the dam as well as to the beach and parking area located on the dam. Loss of a few lives is possible. Accordingly, Lake Intervale Dam is classified as "Significant" hazard.

#### d. Ownership

Lake Intervale Dam is owned and operated by the Lake Intervale Management Association, P.O. Box 221, Boonton, New Jersey 07005.

#### e. Purpose of Dam

The purpose of the dam is the impoundment of a recreational lake facility for the Lake Intervale Management Association.

#### f. Design and Construction History

Reportedly, Lake Intervale Dam was constructed in the late 1940's by a private developer. In 1960 the Lake Intervale Management Association was formed and acquired ownership and responsibility for the dam and its appurtenances.

Reportedly, plans for the dam as it related to the original subdivision are on file with the Township of Parsippany-Troy Hills.

#### g. Normal Operational Procedures

The dam and appurtenances are maintained by the Grounds Committee of the Lake Intervale Management Association. There is no fixed schedule of maintenance; repairs are made as the need arises.

The outlet works, constructed in 1979, reportedly is used to drain the lake for lake maintenance purposes.

The lake was last lowered through the outlet works in September 1979 in order to facilitate dredging operations by the Grounds Committee.

#### 1.3 Pertinent Data

a. Drainage Area 0.53 square miles

#### b. Discharge at Damsite

Maximum flood at damsite Unknown
Outlet Works at pool elevation 10 cfs.
Spillway capacity at top of dam 67 cfs

#### c. Elevation (N.G.V.D.)

| Top of Dam                      | 380.9           |
|---------------------------------|-----------------|
| Maximum pool-design surcharge   | 381.8           |
| Recreation pool                 | 378.7           |
| Spillway crest                  | 378.7           |
| Stream bed at centerline of dam | 374.4           |
| Maximum tailwater               | 377 (Estimated) |

#### d. Reservoir

| Length of maximum pool    |   | 850 feet (Estimated) |
|---------------------------|---|----------------------|
| Length of recreation pool | • | 750 feet (Scaled)    |

#### e. Storage (Acre-feet)

| Recreation pool  | 46  |
|------------------|-----|
| Design surcharge | 114 |
| .Top of dam      | 89  |

#### f. Reservoir Surface (acres)

| Top of dam                      | 19.1 (Estimated) |
|---------------------------------|------------------|
| Maximum pool - design surcharge | 20.0 (Estimated) |
| Recreation pool                 | 10.1             |

#### g. Dam

| Туре                  | Earthfill/Concrete Core |
|-----------------------|-------------------------|
| Length                | 520 feet                |
| Height                | 6.2 feet                |
| Sideslopes - Upstream | 3 horiz. to 1 vert.     |
| - Downstream          | 3 horiz. to 1 vert.     |
| Zoning                | Unknown                 |
| Impervious core       | Concrete Core Wall      |

Cutoff
Grout curtain

Unknown Unknown

h. Diversion and Regulating Tunnel

N.A.

i. Spillway

Type

Length of weir Crest elevation Gates Upstream channel

Downstream channel

Concrete Sharp
Crested Weir
6.0 feet
378.7
Timber Stoplog
Concrete Lined Channel
Natural stream

j. Regulating Outlet

12" diameter gated transite pipe.

#### SECTION 2: ENGINEERING DATA

#### 2.1 Design

No plans or calculations pertaining to the original construction of the dam could be obtained. Drawings prepared in or about 1950 relating to a proposed subdivision which show a plan of the lake reportedly are on file with the Township of Parsippany-Troy Hills.

#### 2.2 Construction

No data or reports pertaining to the construction of the dam are available.

#### 2.3 Operation

Reportedly, informal maintenance reports are on file with the Lake Intervale Management Association.

Data relating to Stream Encroachment Application to the NJDEP for dredging of the lake are available at the NJDEP.

#### 2.4 Evaluation

#### a. Availability

Available engineering data is limited to that which is on file with the Township of Parsippany-Troy Hills and the NJDEP. The files contain drawings relating to a proposed subdivision.

Also, the NJDEP has Stream Encroachment Permit No. 9503 on file which include plans for the current dredging of the lake.

#### b. Adequacy

Available engineering data pertaining to Lake Intervale Dam is not adequate to be of significant assistance to the performance of a Phase I evaluation. A list of absent information is included in paragraph 7.1.b.

#### c. Validity

The validity of engineering data cannot be assessed due to the absence of data.

#### SECTION 3: VISUAL INSPECTION

#### 3.1 Findings

#### a. General

The inspection of Lake Intervale Dam was performed on December 18, 1980 by staff members of Storch Engineers. A copy of the visual inspection check list is contained in Appendix 1. The following procedures were employed for the inspection:

- 1) The embankment of the dam, appurtenant structures and adjacent areas were examined.
- The embankment and accessible appurtenant structures were measured and key elevations determined by surveyor's level.
- 3) The embankment, appurtenant structures and adjacent areas were photographed.
- 4) The downstream flood plain was toured to evaluate downstream development and restricting structures.

#### b. Dam

The right portion of the dam having a length of about 120 feet was generally grass covered with a few trees on its downstream side with sizes of 12 inches to 18 inches and a few trees on its upstream side with sizes about 6 inches. Bushes were also noted on the upstream side. The left portion of the dam, having a length of about 400 feet, was formed by the parking area for a swim club. The area was mostly paved and contained a few small trees on its downstream side. Immediately downstream from the parking area was a paved public road.

The concrete slope protection adjacent to each side of the spillway was in generally satisfactory condition. An eroded area observed adjacent to the slope protection on the downstream side appeared to be the result of pedestrian activity.

#### c. Appurtenant Structures

Concrete surfaces on the spillway structure appeared to be in satisfactory condition. A high water mark noted on the upstream training walls indicated that normal water level is at the top of the observed stoplog. The stoplog appeared to be in generally satisfactory condition, although the rubber strip along its lower edge is somewhat deteriorated and starting to separate from the wood. A temporary plastic pipe was observed in place in the spillway, apparently used in connection with the dewatering of the lake by pumping. The condition of the footbridge spanning the spillway appeared to be good. The wood appeared to be recent and the chain link fence railing appeared to be in good condition.

The upstream end of the outlet pipe was observed protruding from the embankment and the downstream end was observed protruding from the bank of the downstream channel. No gate operating mechanism was observed.

A 15-inch concrete pipe was observed protruding through the right bank of the downstream channel immediately downstream from the spillway structure. The function of the pipe could not be assessed.

#### d. Reservoir Area

The reservoir was almost completely surrounded by home sites, most including lake related structures such as walls and docks. The portion of the reservoir shore near the left section of the dam consisted of a swimming area and beach.

Extensive dredging operations were in progress at the time of inspection. The lake was drawn down by use of pumps at the time of inspection.

#### e. Downstream Channel

The downstream channel between the spillway and the Lake Drive bridge consisted of a natural stream with approximately 3 to 4 foot high banks with a few small trees and bushes growing along the banks. The bottom could not be observed because a stilling basin had been created by the placement of boards just upstream from the bridge in connection with the pumping operations. Downstream from the bridge the downstream channel was a straight, uniformly graded stream extending along the rear property lines of the downstream dwellings. It had sideslopes of approximately 2 to 1 and it had a few small trees growing in the side slopes. Its banks were rather high, approximately 6 to 10 feet. The dwellings on either side of the downstream channel were about 10 feet above the invert and appeared to be slightly below the top of the dam.

The confluence of the downstream channel and the Troy Brook is approximately 500 feet downstream of the dam.

#### SECTION 4: OPERATIONAL PROCEDURES

#### 4.1 Procedures

The level of water in Lake Intervale is normally regulated by discharge through the spillway structure. At the time of inspection the lake was in a drawn down condition for the purpose of dredging. Reportedly, the stoplog is installed for the summer months and removed during the winter. In this manner the level of water varies from approximately elevation 378.0 to 378.8 in winter and summer respectively.

The most recent drawdown of the lake occurred in 1979 when the Lake Intervale Management Association siphoned the lake down a total of approximately twenty feet in order to perform dredging operations.

The stoplog has not been in place since September 1979 when the lake was lowered for the purpose of dredging. The lake was drawn down in September 1979 in about 4 days with the 12-inch transite low level outlet works. It was then drawn down to an elevation 15 feet below the normal low level pool by use of by-pass pumping which remained in use until dredging operations were reportedly completed on December 31, 1980.

#### 4.2 Maintenance of the Dam

Reportedly, maintenance is performed on an "as needed" basis. The Lake Intervale Management Association Grounds Committee inspects the dam on a yearly basis and performs repairs, if necessary.

The timber foot bridge was reportedly repaired in the summer of 1980.

#### 4.3 Maintenance of Operating Facilities

Reportedly, the 12-inch transite outlet works was constructed in 1978 and functions properly. It was not physically operated as part of this inspection.

#### 4.4. Description of Warning System

Reportedly, no warning system is currently in use for the dam.

#### 4.5 Evaluation of Operational Adequacy

The operation of the dam has been successful to the extent that the dam reportedly has not been overtopped.

Although maintenance has been good in some areas, some aspects of dam maintenance have not been adequately performed, including the following:

- 1) Clusters of small trees and brush on the embankment not removed.
- 2) Eroded area on downstream side of embankment not repaired.

#### SECTION 5: HYDRAULIC/HYDROLOGIC

#### 5.1 Evaluation of Features

#### a. Design Data

The quantity of storm water runoff that the spillway should be able to handle is based on the size and hazard classification of the dam. This runoff quantity, called the spillway design flood (SDF), is described in terms of return frequency or probable maximum flood (PMF) depending on the extent of the dam's size and potential hazard. According to the "Recommended Guidelines for Safety Inspection of Dams" published by the U.S. Army Corps of Engineers, the SDF for Lake Intervale Dam falls in a range of 100-year frequency to 1/2 PMF. In this case, the low end of the range, 100-year frequency, is chosen since the factors used to selct size and hazard classification are on the low side of their respective ranges.

The SDF peak computed for Lake Intervale Dam is 713 c.f.s. This value is derived from the 100-year flood hydrograph computed by the use of the HEC-1-DAM Flood Hydrograph Computer Program using the Soil Conservation Service triangular unit hydrograph with curvilinear transformation. Hydrologic computations and computer output are contained in Appendix 4.

The spillway discharge rates were computed by the use of weir and orifice flow formulae appropriate for the configuration of the spillway structure. The total spillway discharge with lake level equal to the top of the dam was computed to be 67 c.f.s. The SDF was routed through the dam by use of the HEC-1-DAM computer program using the modified Puls Method. In routing the SDF, it was found that the dam crest would be

overtopped by a depth of 0.9 foot. Accordingly, the subject spillway is assessed as being inadequate in accordance with criteria developed by the U.S. Army Corps of Engineers.

A dam breach analysis was then performed using a trapezoidal breach section with bottom length of 25 feet and sideslopes of 1 horizontal to 1 vertical. The breach peak outflow was computed to be 1340 c.f.s. Dam breach computations are contained in Appendix 4.

#### b. Experience Data

Reportedly, the dam has not been overtopped since its construction.

#### c. Visual Observation

No evidence was found at the time of inspection that would indicate that the dam had been overtopped.

#### d. Overtopping Potential

As indicated in paragraph 5.1.a. a storm of magnitude equal to the SDF would cause overtopping of the dam by a depth of 0.9 foot over the crest of the dam. The spillway is capable of passing approximately 9 percent of the SDF with the lake level equal to the top of dam.

#### e. Drawdown Data

Drawdown of the lake is accomplished by opening the gated 12-inch outlet pipe. Total time for drawdown is estimated to be approximately 3 days. (See Appendix 4.)

#### SECTION 6: STRUCTURAL STABILITY

#### 6.1 Evaluation of Structural Stability

#### a. Visual Observations

The dam appeared, at the time of inspection to be outwardly structurally sound with no evidence of embankment cracks or distress. No evidence of seepage was observed. Due to the extremely drawndown condition of the dam, a seepage evaluation cannot be performed.

#### b. Generalized Soils Description

The generalized soils description of the dam site consists of recent alluvium, composed of stratified materials deposited by streams, overlying glacial ground moraine deposited during the Wisconsin Glaciation. The glacial moraine and kames are composed of silts and silty sands and overlie shale and sandstone known as the Brunswick Formation in the Geologic Map of New Jersey prepared by Lewis and Kummel.

#### c. Design and Construction Data

Analysis of structural stability and construction data for the embankment are not available.

#### d. Operating Records

No operating records are available for the dam. The water level of Lake Intervale is not monitored.

#### e. Post-Construction Changes

The major post-construction change at the dam site is the extensive removal of soil from the bottom of Lake Intervale. Lake dredging operations with the lake drawn down were in progress at the time of inspection.

#### f. Seismic Stability

Lake Intervale Dam is located in Seismic Zone 1 as defined in "Recommended Guidelines for Safety Inspection of Dams" which is a zone of very low seismic activity. Experience indicates that dams in Seismic Zone 1 will have adequate stability under seismic loading conditions if they have adequate stability under static loading conditions. Lake Intervale Dam appeared to be stable at the time of inspection.

#### SECTION 7: ASSESSMENT AND RECOMMENDATIONS

#### 7.1 Dam Assessment

#### a. Safety

Based on hydraulic and hydrologic analyses outlined in Section 5 and Appendix 4, the spillway of Lake Intervale Dam is assessed as being inadequate. The spillway is not able to pass the SDF without an overtopping of the dam.

The embankment appeared, at the time of inspection, to be outwardly stable.

#### b. Adequacy of Information

Information sources for this report include 1) field inspections,
2) USGS quadrangle, and 3) consultation with personnel of the
- Lake Intervale Management Association. The information obtained is sufficient to allow a Phase I assessment as outlined in "Recommended Guidelines for Safety Inspection of Dams."

Some of the absent data are as follows:

- 1. Construction and as-built drawings.
- 2. Description of fill material for embankment.
- 3. Design computations and reports.
- 4. Soils report for the site.
- 5. Inspection reports.

#### c. Necessity for Additional Data/Evaluation

Although some data pertaining to Lake Intervale are not available, additional data are not considered imperative for this Phase I evaluation.

#### 7.2 Recommendations

#### a. Remedial Measures

Based on hydraulic and hydrologic analyses outlined in paragraph 5.1.a, the spillway is considered to be inadequate. It is therefore recommended that a professional engineer experienced in the design and construction of dams be engaged in the near future to perform more accurate hydraulic and hydrologic analyses relating to spillway capacity. Based on the findings of these analyses, the need for and type of remedial measures should be determined and then implemented.

In addition, it is recommended that the following remedial measures be undertaken by the owner in the near future.

- Trees and adverse vegetation on the dam embankment should be removed.
- 2) The eroded area on the downstream side of the embarkment should be properly filled and stabilized.

#### b. Maintenance

In the future, the owner of the dam should develop written operating procedures and a periodic maintenance plan to ensure the safety of the dam.

#### c. Additional Studies

When the water level returns to its normal level, the dam and its appurtenances should be inspected for seepage.

PLATES

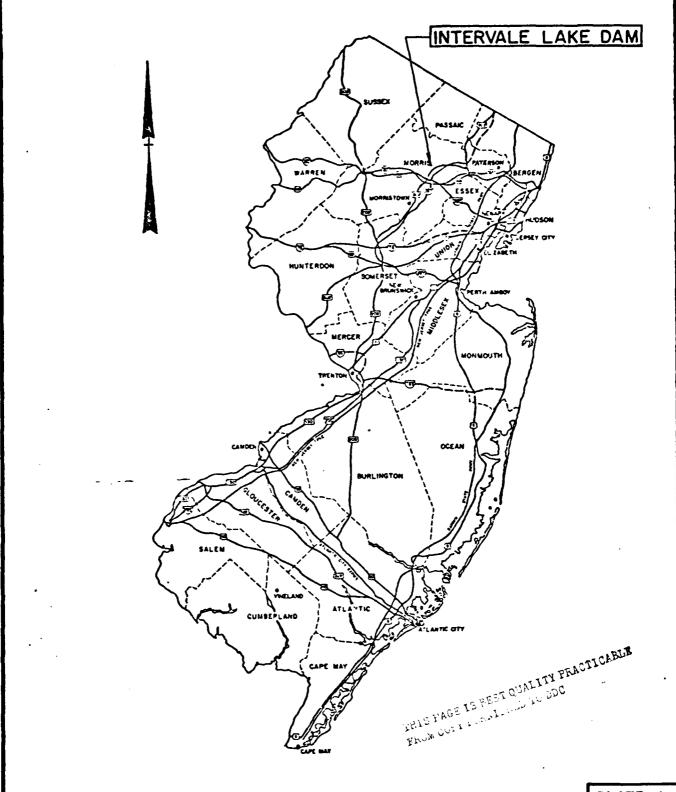


PLATE I

STORCH ENGINEERS
FLORHAM PARK, NEW JERSEY

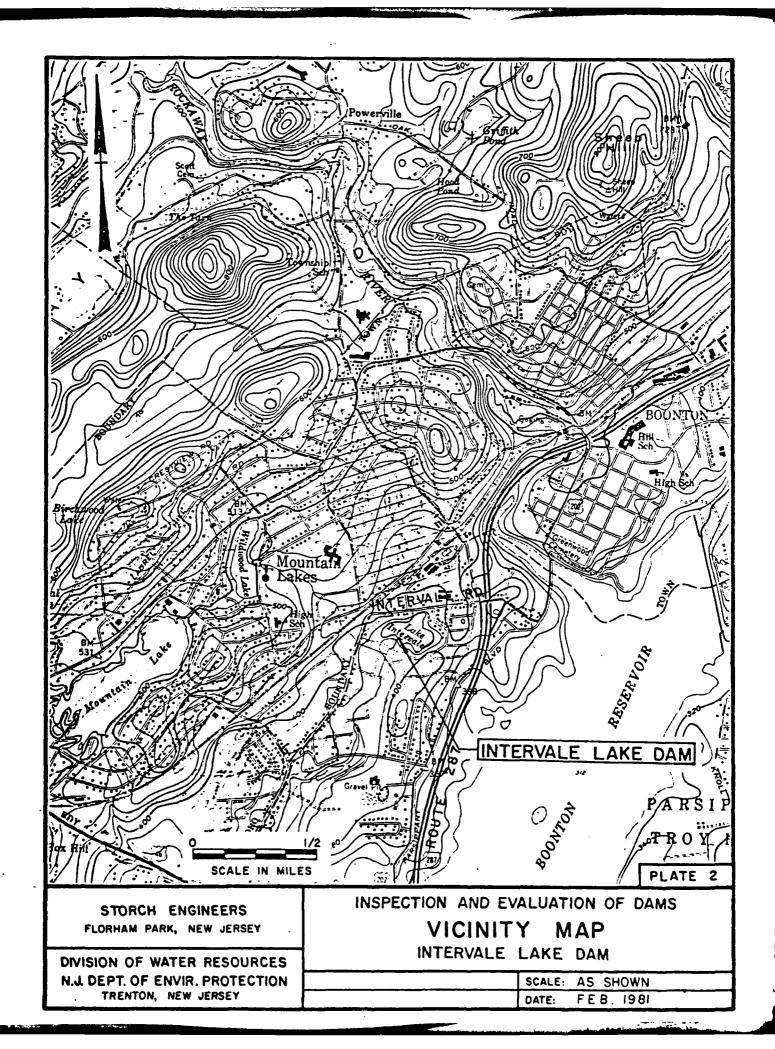
DIVISION OF WATER RESOURCES
N.1 DEPT. OF ENVIR PROTECTION
TRENTON, NEW JERSEY

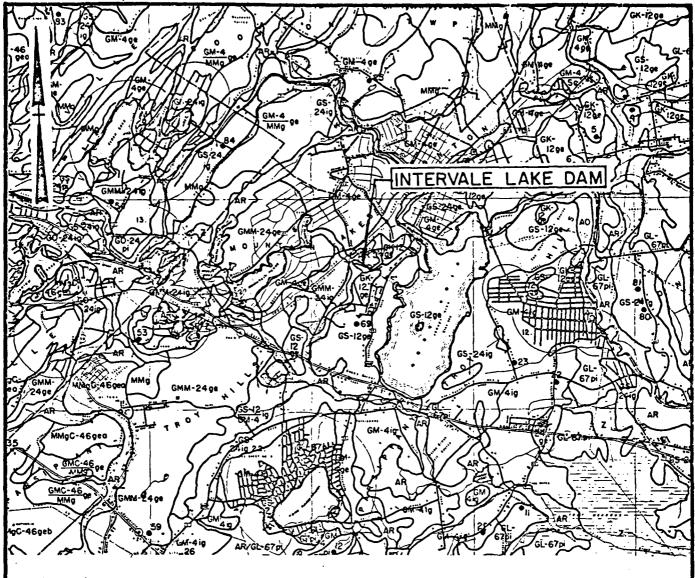
INSPECTION AND EVALUATION OF DAMS

KEY MAP

INTERVALE LAKE DAM

SCALE: NONE DATE: FEB.1981





#### Legend

AR Recent alluvium; composed of stratified materials deposited

by streams.

GK-12 Glacial kames; composed of stratified materials deposited during

the Wisconsin glacial period.

GM-4 Glacial ground moraine; composed of unstratified material

deposited during the Wisconsin glaciation.

Note: Information taken from: Rutgers University Engineering Soil Survey

of New Jersey, Report No. 9, Morris County, November 1953 and Geologic Map of New Jersey prepared by J. V. Lewis and H. Kummel 1910-1912, revised by H. B. Kummel 1931 and M. Johnson 1950.

PLATE 3

STORCH ENGINEERS
FLORHAM PARK, NEW JERSEY.

DIVISION OF WATER RESOURCES
N.J. DEPT. OF ENVIR. PROTECTION
TRENTON, NEW JERSEY.

INSPECTION AND EVALUATION OF DAMS

SOIL MAP

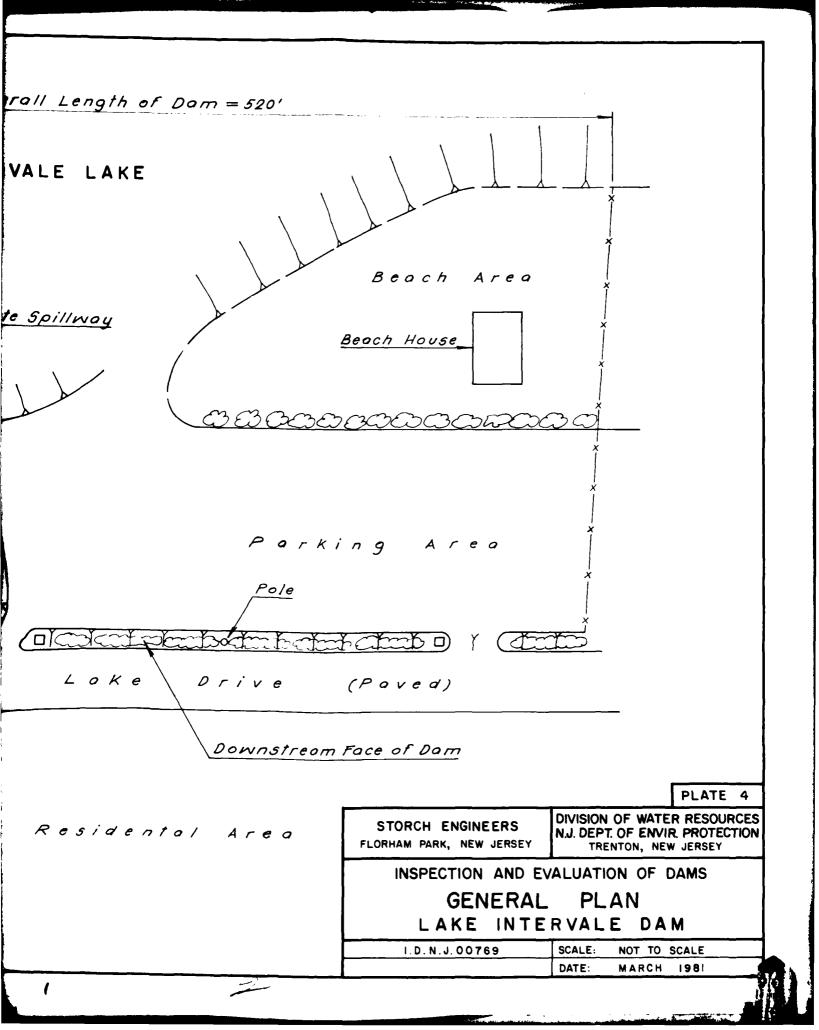
INTERVALE LAKE DAM

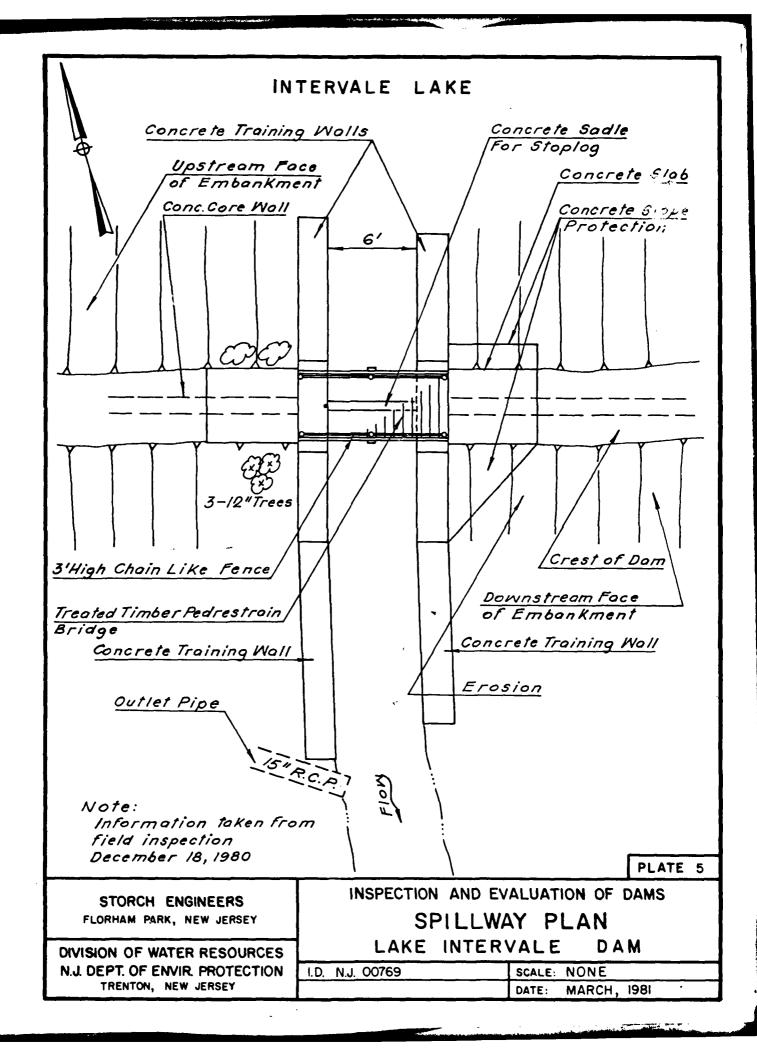
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DATE: FEB.1981

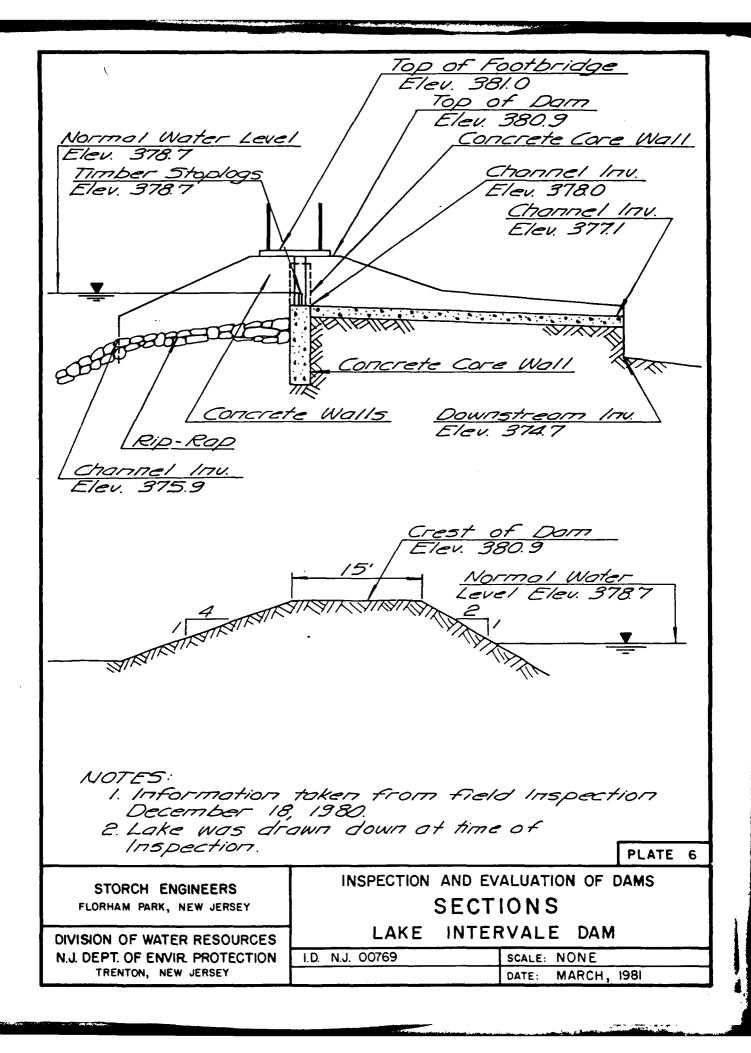
Cverall INTERVAL Concrete Sp Downstream Face of Dom Downstream Channel

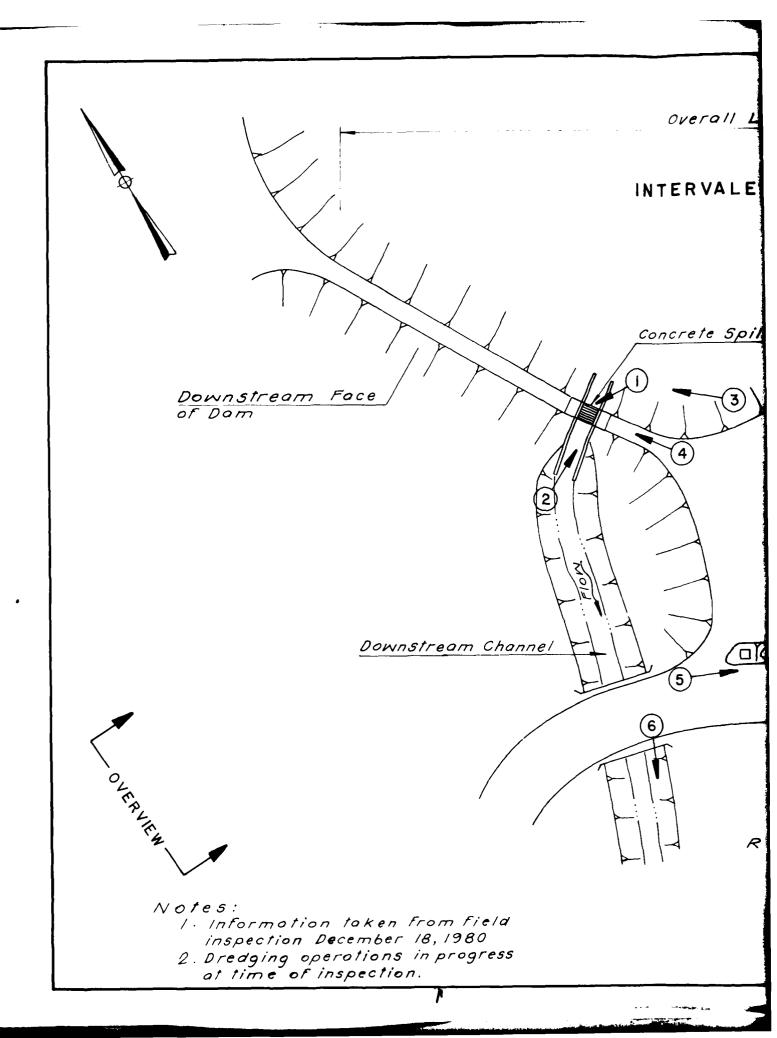
#### Notes:

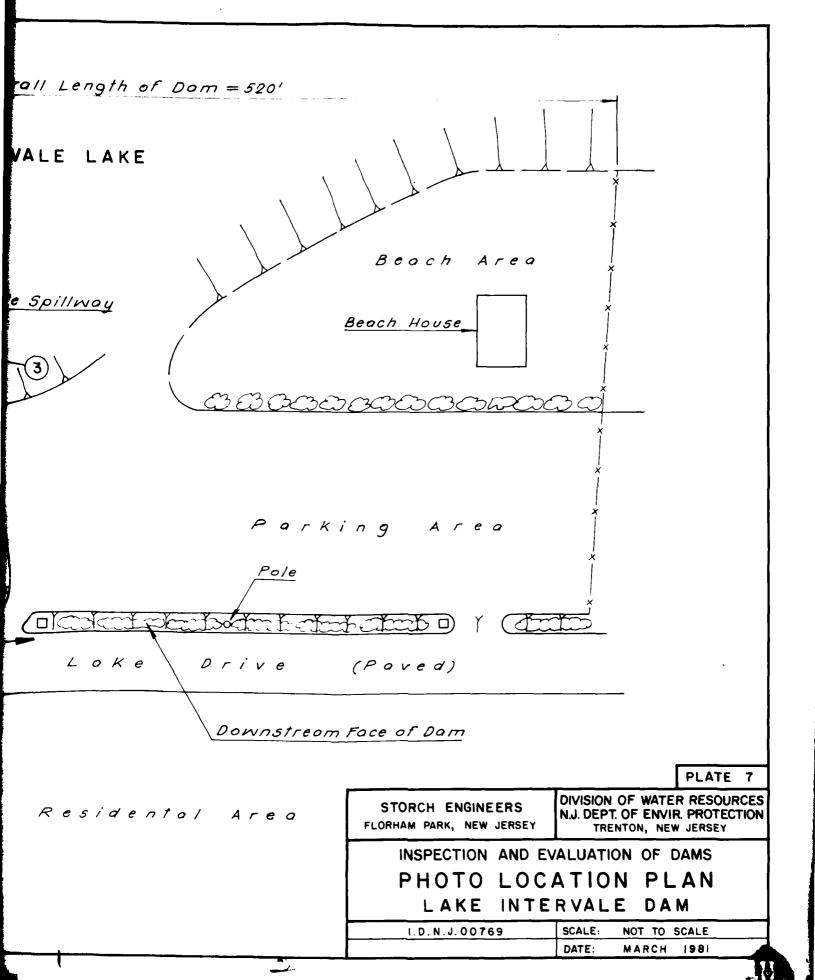
- 1. Information taken from field
- inspection December 18, 1980
  2. Dredging operations in progress at time of inspection.











### APPENDIX 1

Check List - Visual Inspection
-- Check List - Engineering Data

Check List

Visual Inspection

Phase I

| Name of Dam  | Lake Intervale Dam  | County Morris   | State N.J.                            | Coordinators NJDEP   | 1        |
|--|---|---|---------------------------------------|----------------------|----------|
| Date(s) Inspection 12/18/80  | ion 12/18/80  | Weather Cloudy  | Temperature 300F                      |                      |          |
| Pool Elevation a   | Pool Elevation at time of Inspection 345 (approx.) M.S.L.<br>(Lake dredged & drawn do | n 345 (approx.) M.S.L.<br>(Lake dredged & drawn down) | Tailwater at Time of Inspection 373.5 | Inspection 373.5 M.S | <u> </u> |
| Inspection Personnel:  | onnel:  |   |                                       | ,                    |          |
| John Gribbin<br>Charles Osterkorn<br>Daniel Buckelew   |   | Andrew Polperio<br>Richard McDermott                  |                                       |                      |          |
| Out of the state o | ;   | John Gribbin  | Recorder                              | · .                  | •        |

## **FMRANKMFNT**

|   | EMBANKMENT  |   |
|---|---|---|
| VISUAL EXAMINATION OF                                       | OBSERVATIONS  | REMARKS OR RECOMMENDATIONS  |
| GENERAL   | Right section of embankment generally grass covered with a few trees (12" to 18") on downstream side and bushes and a few trees (6") on upstream side. Most of left section of embankment paved (parking area) with a few small trees on downstream side. | Trees should be removed.  |
| JUNCTION OF EMBANKMENT<br>AND ABUTMENT, SPILLWAY<br>AND DAM | Junctions appeared stable.  | ·   |
| ANY NOTICEABLE SEEPAGE                                      | None observed   | Lake drawn down:<br>Seepage not possible under draw<br>down condition.                                    |
| STAFF GAGE AND RECORDER                                     | None observed   |   |
| DRAINS  | Outlet end of 15" conc. pipe observed protruding through right bank of downstream channel immediately downstream from spillway structure.   | Function of pipe could not be assessed. Pipe could possibly be toe drain for right portion of embankment. |
|   |   |   |

## **EMBANKMENT**

| SURFACE CRACKS CRACKING AT OR BEYOND THE TOE   | None observed  No sloughing observed.  Erosion observed on downstream side of embankment adjacent to conc.  | Froded area should be filled and properly stabilized. |
|--|---|---|
| SEUUGHING UK EKUSIUN UF EMBANKMENT AND ABUTMENT SLOPES  VERTICAL AND HORIZONTAL ALIGNMENT OF THE CREST  RIPRAP | Wertical: varies  Horizontal: irregular  None observed.  Conc. slab slope protection observed on crest adjacent to spillway and on upstream and downstream side left of spillway for distance of 5' appeared to be in satisfactory condition. |   |

## OUTLET WORKS

|  | OUTLET WORKS   |                            |
|--|--|----------------------------|
| VISUAL EXAMINATION OF                  | OBSERVATIONS   | REMARKS OR RECOMMENDATIONS |
| CONCRETE SURFACES IN<br>OUTLET CONDUIT | l2 inch transite pipe generally could not be observed.<br>Discharge end protruding through bank of downstream<br>channel appeared in generally satisfactory condition. | ·                          |
| INTAKE STRUCTURE                       | Not observed.  | •                          |
| OUTLET STRUCTURE                       | N.A.   |                            |
| OUTLET CHANNEL                         | Outlet works discharge directly into downstream channel.   |                            |
| GATE AND GATE HOUSING                  | Not observed.  |                            |
|  |  |                            |

### SPILLWAY

| VISUAL EXAMINATION OF | OBSERVATIONS  | REMARKS OR RECOMMENDATIONS  |
|-----------------------|---|---|
| WEIR                  | Timber stoplog forming weir in generally satisfactory condition with rubber seal deteriorated. Conc. saddle upon which stoplog rests was in satisfactory condition. | Stoplog not functioning at time of inspection due to draw down condition of lake. Stoplog should be repaired. |
| TRAINING WALLS        | Appeared in satisfactory condition.   |   |
| DISCHARGE CHANNEL     | Formed by cond. training walls appeared in satisfactory condition.  | •   |
| BRIDGE                | Timbers forming pedestrian bridges appeared in good<br>condition. Chain link fence railings also in good<br>condition.  |   |
|                       |   |   |

## INSTRUMENTATION

|                       | INSTRUMENTATION |                            |
|-----------------------|-----------------|----------------------------|
| VISUAL EXAMINATION OF | OBSERVATIONS    | REMARKS OR RECOMMENDATIONS |
| MONUMENTATION/SURVEYS | None            | •                          |
| OBSERVATION WELLS     | None            | •                          |
| WEIRS                 | None            |                            |
| P1EZOMETERS           | None            | ·                          |
| OTHER                 | •               |                            |
|                       |                 |                            |

### RESERVOIR

| SEDIMENTATION OF Shore slopes are moderate to flit. Area is completely developed for residential use.  SEDIMENTATION  None. Extensive dredging operations in progress at time of inspection. Invert of lake appeared about 30 below dam crest. Lake draw down by pumps at time of inspection. Homesites where observed around entire lake area.  STRUCTURES ALONG Walls and docks.  BANKS |                             | RESERVOIR  |                            |
|---|-----------------------------|--|----------------------------|
|   | VISUAL EXAMINATION OF       | OBSERVATIONS   | REMARKS OR RECOMMENDATIONS |
|   | SLOPES                      |  |                            |
| Homesites were observed around entire lake Homesites included lake related structures walls and docks.  | SEDIMENTATION               | None. Extensive dredging operations in progress at time of inspection. Invert of lake appeared about 30' below dam crest. Lake draw down by pumps at time of inspection. | •                          |
|   | STRUCTURES ALONG<br>BANKS   | Homesites were observed around entire lake<br>Homesites included lake related structures<br>walls and docks.   |                            |
|   |                             |  |                            |
|   | ing a week with the file of |  |                            |

# DOWNSTREAM CHANNEL

|   | DUMNSIKEAM CHANNEL   | •   |
|---|--|---|
| VISUAL EXAMINATION OF                       | OBSERVATIONS   | REMARKS OR RECOMMENDATIONS                                    |
| CONDITION<br>(OBSTRUÇTION,<br>DEBRIS, ETC.) | Channel is well graded and straight. Temporary timber weir was in place immediately upstream from road bridge. Weir appeared to be related to dredging and pumping operations. | Discharge from pumping of lake<br>entered downstream channel. |
| SLOPES                                      | Both banks had slopes of about 2 horiz. to l vert. and<br>were about 6 to 10 feet high.  |   |
| STRUCTURES ALONG<br>BANKS                   | Road bridge about 150' downstream. Several dwellings<br>adjacent to channel downstream from bridge, min. 8'<br>above stream invert.  | Channel extends along rear property<br>lines of homesites.    |
| •   |  |   |
|   |  |   |

## CHECK LIST ENGINEERING DATA DESIGN, CONSTRUCTION, OPERATION

| ITEM                                |                   | REMARKS   |
|-------------------------------------|-------------------|---|
|                                     |                   |   |
| DAM                                 | PLAN              | Available in NJDEP Files - Stream Encroachment Permit #9503 |
|                                     | SECTIONS          |   |
| SPILLWAY -                          | PLAN              | Not Available   |
|                                     | SECTIONS          |   |
|                                     | DETAILS           |   |
| OPERATING EQUIPMENT PLANS & DETAILS | I PMENT<br>LS     | •   |
| OUTLETS -                           | PLAN              | Not Available   |
|                                     | DETAILS           |   |
|                                     | CONSTRAINTS       |   |
|                                     | DISCHARGE RATINGS |   |
| HYDRAULIC/HYDROLOGIC DATA           | ROLOGIC DATA      | Not Available   |
| RAINFALL/RESERVOIR RECORDS          | RVOIR RECORDS     | Not Available   |
| CONSTRUCTION HISTORY                | HISTORY           | Not Available   |

Available in DEP files. Drawings prepared in or about 1950 relating to proposed subdivision show a plan of the lake, on file with the Township of Parsippany-Troy Hills.

LOCATION MAP

|         | •               | •               | •   |   |                                  |
|---------|-----------------|-----------------|---|---|----------------------------------|
| REMARKS | Not Available   | Not Available   | Not Available   | Not Available   | Not Available                    |
| ITEM    | DESIGN REPORTS: | GEOLOGY REPORTS | DESIGN COMPUTATIONS<br>HYDROLOGY & HYDRAULICS<br>DAM INSTABILITY<br>SEEPAGE STUDIES | MATERIALS INVESTIGATIONS<br>BORING RECORDS<br>LABORATORY<br>FIELD | POST-CONSTRUCTION SURVEYS OF DAM |

| ITEM  | REMARKS                                     |
|---|---|
| MONITORING SYSTEMS  | Not Available                               |
| MODIFICATIONS   | Not Available                               |
| HIGH POOL RECORDS   | Not Available                               |
| POST CONSTRUCTION ENGINEERING<br>STUDIES AND REPORTS        | Stream Encroachment Application-NJDEP files |
| PRIOR ACCIDENTS OR FAILURE OF DAM<br>DESCRIPTION<br>REPORTS | Not Available                               |

Informal maintenance reports on file with the Lake Intervale Management Association

MAINTENANCE OPERATION RECORDS APPENDIX 2

Photographs



PHOTO 1

CREST AND RIGHT TRAINING WALL OF SPILLWAY



PHOTO 2

DOWNSTREAM SIDE OF SPILLWAY

LAKE INTERVALE DAM
18 DECEMBER 1980



PHOTO 3

UPSTREAM SIDE OF DAM AND SPILLWAY



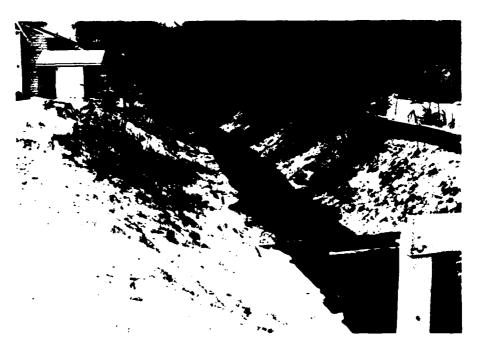
PHOTO 4
CREST OF DAM

LAKE INTERVALE DAM
18 DECEMBER 1980



PHOTO 5

DOWNSTREAM SIDE OF DAM-LEFT SECTION



РНОТО 6

DOWNSTREAM CHANNEL

LAKE INTERVALE DAM

18 DECEMBER 1980

APPENDIX 3

Engineering Data

### CHECK LIST

### HYDROLOGIC AND HYDRAULIC DATA

### ENGINEERING DATA

| DRAINAGE /   | AREA CHARACTERISTIC | S: Residential                              |  |  |  |
|--|---------------------|---|--|--|--|
| ELEVATION TOP NORMAL POOL (STORAGE CAPACITY): 378.7 (46 acre-ft) |                     |   |  |  |  |
| ELEVATION TOP FLOOD CONTROL POOL (STORAGE CAPACITY): N/A         |                     |   |  |  |  |
| ELEVATION  | MAXIMUM DESIGN POO  | DL:381.8                                    |  |  |  |
| ELEVATION  | TOP DAM:            | 380.9                                       |  |  |  |
| SPILLWAY   | CREST:              | Controlled Weir (Stoplogs)                  |  |  |  |
| a.   | Elevation 378.      | .7  |  |  |  |
| b.   | Type Shar           | rp_Crested Weir                             |  |  |  |
| с.   | Width 0.1           | feet  |  |  |  |
| d.   | Length 6.0          | feet  |  |  |  |
| е.   | Location Spillover  | Center of dam                               |  |  |  |
| f.   | Number and Type of  | Gates One stoplog                           |  |  |  |
| OUTLET WO  | RKS:                |   |  |  |  |
|  |                     | ch Transite Pipe                            |  |  |  |
| •  |                     | f the Spillway                              |  |  |  |
| c.   | Entrance Invert     | 374.0                                       |  |  |  |
| d.   | Exit Invert         | 374.0                                       |  |  |  |
| e.   | Emergency Draindov  | wn Facilities: Remove Stoplog and open gate |  |  |  |
| HYDOMETEO  | ROLOGICAL GAGES:    | None  |  |  |  |
| a.   | Туре                | N/A   |  |  |  |
| b.   | Location            | N/A   |  |  |  |
| с.   | Records             | N/A   |  |  |  |
| MAXIMUM N  | ON-DAMAGING DISCHA  | RGE:  |  |  |  |
| (Lake Stage Equal to Top of Dam) 67 c.f.s.                       |                     |   |  |  |  |

APPENDIX 4

\_Hydraulic/Hydrologic Computations

| STORCH ENGIN                                     | INTERU             | IALE LAKE                              | Dam       |                   | pet/_ of <u>/3</u><br>Date_ <u>2-25-8/</u> |
|--|--------------------|--|-----------|-------------------|--|
|  |                    |  |           |                   | Date 2/27/81                               |
|  |                    | !                                      |           |                   |  |
|  |                    |  | !         |                   |  |
|  |                    | HYDROL                                 | OG Y      |                   |  |
|  |                    |  |           |                   |  |
|  | HYDROLO            | ogic Analy                             | 1515      |                   |  |
|  |                    |  |           |                   |  |
|  | Runoff             | hydrogr                                | aph wi    | Il be deve        | Loped                                      |
| by   | HEC - 1 -          | DAM USING                              | SCS       | triangular        | ·  |
|  |                    | J                                      |           | J J               |  |
| h  | ydrograph u        | with the                               | curvili   | near frans        | formation                                  |
|  | , , ,              |  |           |                   |  |
| <u> </u>   | Jacobs An          |  | 53 50 r   | M i               | · · · · · · · · · · · · · · · · · · ·      |
|  | rainage Ar         | JEA - 013                              | 70 04, 11 |                   |  |
|  |                    | 1                                      | :         |                   | <del></del>                                |
|  | nfiltration        | 1 Data                                 |           |                   |  |
|  |                    |  |           |                   |  |
|  | Initial<br>Constan | tatiltrat                              | 104       | 1.5 in<br>0.15 in | · /  |
| ······································           | Constan            | T 1171                                 | 1710N     | U.15 In           | /nr  |
|  |                    |  |           |                   |  |
| Ti   | me of Con          | centration                             | n (ta)    | (Method #         | 1)   |
|  |                    |  |           |                   |  |
| The second section is the second common new con- | R. 606 T           | 2 56                                   |           | M                 |  |
| · - · · · ·                                      | By SCS TH          | <u> </u>                               |           | and channe        | Overland Flow                              |
|  | DUERLAND           | Flows:                                 |           | ang channe        | 21. 3. 10w.                                |
|  | L                  | = 6,000'                               |           |                   | <u> </u>                                   |
|  | L<br>A             | ELEV = 3                               | 20'       |                   |  |
|  |                    | 5 = 5.3370                             | • • •     |                   | <del></del>                                |
|  | 1                  | ــــــــــــــــــــــــــــــــــــــ |           | 2.96              | 110  |

| STORCH ENGI                                  | INTERVALE LAKE DAM   | Sheet <u>2</u> of <u>/</u><br>Made By <u>JLP</u> Date <u>2-25-</u>   |
|--|--|--|
| Project                                      | INICHUALE LAND DAM   | -  |
|  |  | Chkd By <u>JG</u> Date <u>2/27/</u>  |
|  |  |  |
| · · · · · · · · · · · · · · · · · · ·        |  | (m 11 1 # a)   |
|  | Time of Concentration  | (Method #2)  |
|  |  |  |
|  | by KERby Pg. 14.34   | · "Handbook of Applied   |
|  | 0 0 10   | Hydrology" Chow.   |
|  |  | , 00   |
| i  |  | <del></del>  |
| <u> :                                   </u> | $T_c = \frac{2.14}{2/3} \frac{Ln}{1}$  | To = Time of Concentrati   |
| · · · · · · · · · · · · · · · · · · ·        | c = 73 TS  | in min.  |
|  | V -  | L= Length o+ Overlan   |
|  |  | flow in ft.  |
|  |  | S=Slope  |
| <del></del>                                  |  | n = 0,4 (roughness Coe   |
|  |  |  |
|  | 7 L. 1 Cla   |  |
|  | DUERLAND Flow:   |  |
|  | -  | )00'<br>E22  |
|  | S = 0  |  |
|  | n = 0.4  | 1.04 He.   |
|  |  | 1.04 Hz.   |
|  |  |  |
|  | TIME of Concer   | tration (Method #3)  |
|  |  |  |
|  | N.J. Highway Authori   | ty Nomograph   |
|  | <u> </u>   | · · · · · · · · · · · · · · · · · · ·  |
|  | and a second   | and the same and the same of t |
|  | DUERLAND Flow:   |  |
| . , , ,                                      | and the second of the second o |  |
|  | L= 6,0   | 000',  |
|  |  | 33%  |
|  | Aug. GR  | A  |
|  | $\mu$  | 0.90 Hr.   |

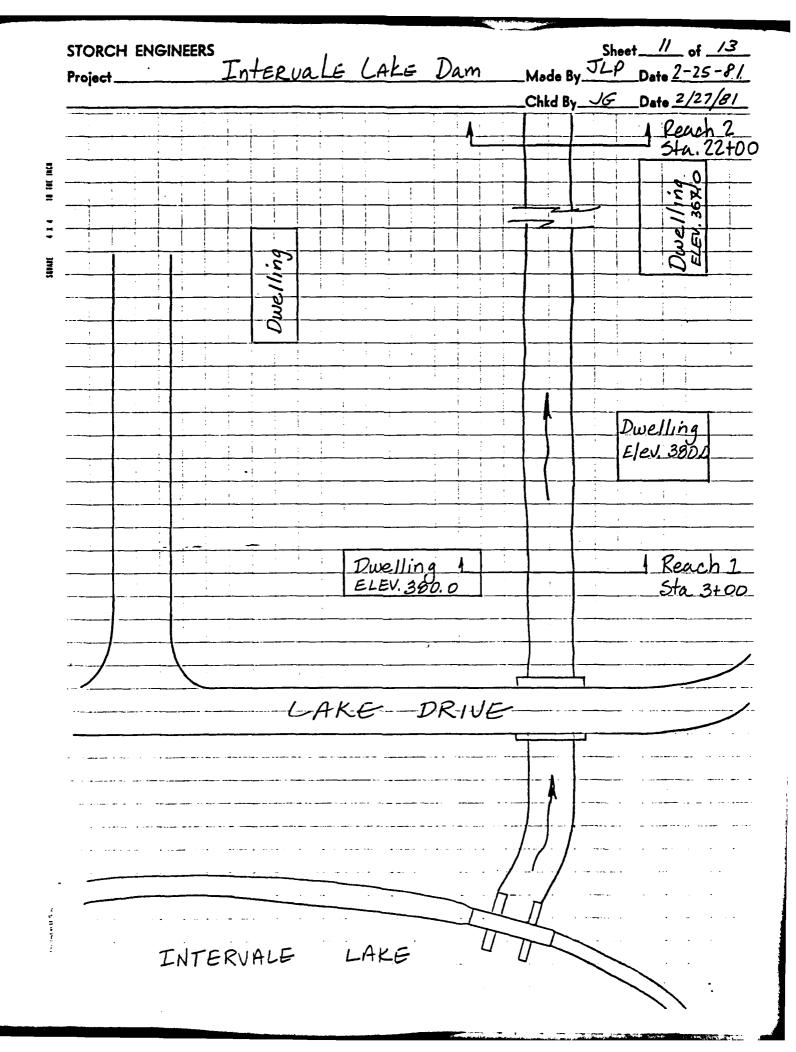
| oiect Intervale Lake Dam     |                   | et 4 of 13                            |
|------------------------------|-------------------|---------------------------------------|
| oject                        |                   | _Date _2-25-8/                        |
|                              | Chkd By <i>JG</i> | Date 2/27/81                          |
|                              |                   |                                       |
| Precipitation_               |                   |                                       |
|                              |                   |                                       |
|                              | 6. 1. 1. 1.       |                                       |
| 24 HOUR - 100 YEAR Rainstorm | Distribution      | <u>Pn</u>                             |
|                              |                   |                                       |
|                              |                   |                                       |
| For Intervale LAKE           | Dam_              | · · · · · · · · · · · · · · · · · · · |
| Time (hr.) Rain (            | (Inches)          |                                       |
|                              | <u> </u>          | !                                     |
| 0.0                          | 75                | :                                     |
| 2 0.07                       |                   |                                       |
| 3 0.07                       |                   | :                                     |
| 4 0.07                       |                   |                                       |
| 5 0.07                       |                   |                                       |
| 0.07                         |                   |                                       |
| 7 0.07                       |                   |                                       |
| 8 0.075                      | 5                 |                                       |
| 9 0.075                      | 5                 | · · · · · · · · · · · · · · · · · · · |
| 10 0.07:                     | <u> </u>          |                                       |
| <u> </u>                     | <u> </u>          |                                       |
| 12 0.075                     |                   |                                       |
| 1.3                          |                   |                                       |
| 14 0.15                      | <del></del>       |                                       |
| 15 0.15                      |                   |                                       |
| 0.33                         |                   | · · · · · · · · · · · · · · · · · · · |
| 0,65                         |                   | · · · · · · · · · · · · · · · · · · · |
| 3.00                         | ,                 |                                       |
| 19                           |                   | • • • • • •                           |
| 20 0.33                      |                   | • • •                                 |
| 21 0.33<br>72 0.15           | • • • • • • • • • |                                       |
| 22<br>23<br>0.15             |                   |                                       |
| 24 0.15                      |                   |                                       |
| <u>0.13</u><br>7.12          |                   |                                       |

FROM TP40 U.S. Weather Bureau

| STORCH I | ENGINEERS<br>Intervale Lake  |   | et <u>5</u> of <u>/3</u>              |
|----------|--|---|---------------------------------------|
| Project  | LNTERVALE CAPE   | -   | Date 2 -25 -21                        |
|          |  | Chkd By VG                                  | _Date 2/27/81                         |
|          |  |   |                                       |
| i i      |  |   | <del> </del>                          |
|          | ELEVATION  | - Storage Table                             |                                       |
| 1        |  |   |                                       |
|          | Information -  | from U.S.G.S. Maps                          |                                       |
|          |  |   |                                       |
|          |  | T   |                                       |
|          | ELEV. (M.S.L.)   | Storage (Acre-ft.)                          |                                       |
|          |  |   | :                                     |
|          | 374.4  |   |                                       |
|          | 378.0  | 35,8  |                                       |
|          | 0.701.0  | 09,   | · · · · · · · · · · · · · · · · · · · |
|          | 380.0  | 64. 2                                       |                                       |
|          | 1.02.0   | 614.2                                       | <del></del>                           |
| ·        | 400.0  | 614. 2                                      | · · · · · · · · · · · · · · · · · · · |
|          |  |   |                                       |
|          |  |   |                                       |
|          | ·  |   |                                       |
|          |  |   |                                       |
| <u> </u> | HEC 7 - DAM Comp   | uter Program will de                        | evelon                                |
|          | and the second s |   |                                       |
|          | storage capacity   | from storage volumes                        | <b>E</b> '                            |
| <br>     | elevations. Storage<br>lake dredging will  | e below elev. 374.4 d<br>I not be included. | ve to                                 |
|          |  | en from USGS Qua                            |                                       |

|   | -1-1 5-17  |      | WEIR |              | Oi   | PIFICE |          |         |
|---|------------|------|------|--------------|------|--------|----------|---------|
|   | ELEV. [F1] | Н    | С    | Q            | #    | Q      | . QTOTAL |         |
|   | 378.7      | θ-   | -0   | <del> </del> |      |        | θ        |         |
|   | 379.0      | -0.3 | ŀ    | 3.3          |      |        | 3,3      |         |
|   | 379.5      | 0.8  | 3.33 | 14.3         |      |        | 14;3     |         |
|   | 380.0      | 1.3  | 3.33 | 29.6         |      |        | 29.6     |         |
|   | 380.9      | -2.2 | 3.33 | 65.2_        | -/,/ | - 66.6 | 66.6     |         |
| - | 382.0      |      |      |              | 2.2  | 94.3   | 94.3     |         |
|   | 383.0      |      |      |              | 3.2  | 113.7  | //3 .7   |         |
|   | 384,0      |      |      |              | 4.2  | -130.3 | 130.3    | • • • · |

| . [      |              |             |             |              | 1  |              | 1  |          |   | Ka B      | <u>γ_</u>  | <del>-</del>  | _Dat     |              | - 1/   | <u></u>        |
|----------|--------------|-------------|-------------|--------------|--|--------------|--|----------|---|-----------|--|---------------|----------|--------------|--|----------------|
|          |              |             |             |              |  | . !          | <del> </del>                                 |          | <u> </u>                                | +         |  | $\dashv$      | +        | <del></del>  | <del>-  </del>                                   | <u></u>        |
|          |              |             | BRE         | ACH          | AL   | ALYS         | 515  |          |   |           |  |               |          |              |  |                |
|          |              |             |             | ++-          | + -  |              |  |          |   | 1         |  | -             | 1        | <u> </u>     |  | !              |
| _        |              |             |             | 1112         | <del>                                     </del> | - 01         | <del> </del>                                 |          |   | +-        |  |               | -        | -            |  | <u> </u>       |
|          | A            | SKEH        | CH          | 144D1        | ROGR   | APH          | <u>  W</u>                                   | <u> </u> | ······································· | E_        | 00   | MPI           | ITE      | D.           | BY   |                |
|          | THE          | 4=0         | - 1 -       | DAM          | DP.  | 600          | m  | AN       | 0 1                                     | 011       | TEV  | 7             | 1100     | 115          | 11   | <del>- ;</del> |
| , ,      | 180          | 1100        |             | 0,1,1,1      | 100  | MICH         | <u>                                     </u> | 71.      |   |           | 161  |               | <u> </u> | ינטעי        |  | <del></del>    |
|          | Two          | Dov         | NNS.        | TREA         | m R  | EACH         | les  | B        | Υ .                                     | THE       | 'n   | DOC           | IFI      | ED           |  | :              |
|          |              |             |             |              | ······································           |              |  |          | <i>1</i> :                              | 1         | 1 1  |               |          | 1            |  |                |
|          | PULS         | ME          | ETHO        | OD.          | THE  | ASS          | SUM  | ED       | $\mathcal{B}$                           | REI       | 90H  | - (           | LONS     | DIT          | IDN  | 5              |
| <u> </u> |              |             | :<br>       |              | <u>:</u>   |              | <u>:</u>                                     |          | 1                                       | <u> </u>  | <del>                                     </del> |               | i<br>    | <del>-</del> | <del>                                     </del> | <u>.</u>       |
|          | HRE          | <u> 4</u> 5 |             | ollou        | <u>ゟ;</u>  | · ;          |  |          | <del></del>                             | +-        | <del>!                                    </del> |               |          | :            |  | · ·            |
|          |              |             | <del></del> | <u>·</u>     | <del></del>                                      | <del>i</del> | :  | -        | <del>-</del>                            | -         |  | $\overline{}$ |          | <del>.</del> | i  |                |
|          | 1 7          | 45          | RDF         | ACH          | REG  | 14/<         | - 11   | 1461     | 1                                       | TUO       | <del></del> -                                    | 110           | TEP      |              | <del> </del>                                     |                |
|          |              |             |             |              |  | <u></u>      |  | ית טו    | ~                                       | טיוו      |  | <u>~π</u> _/  | -/       |              |  |                |
|          | <b>'</b> '.5 | URFAL       | 2 <i>E</i>  | FLEV         |  |              |  |          |   |           |  |               | i        |              |  |                |
|          |              | URFAC       | CE.         | ELEV         | ATION  |              |  |          |   |           |  |               | :        | :            |  | <u>·</u>       |
|          |              |             | :           |              | ATION  | RE           | AC   | HES      | <u> </u>                                | <i>38</i> | 0.   | 9.            | :        | :            |  |                |
|          | 2. TI        | ME          | TO          | ELEV<br>DEVI | ATION  | RE           | AC   | HES      | <u> </u>                                | <i>38</i> | 0.   | 9.            |          | :            |  |                |
|          | 2. TI        |             | TO          |              | ATION  | RE           | AC   | HES      | <u> </u>                                | <i>38</i> | 0.   | 9.            |          | :            |  |                |
|          | 2. TI        | ME          | TO          |              | ATION  | RE           | AC   | HES      | <u> </u>                                | <i>38</i> | 0.   | 9.            |          |              |  |                |
|          | 2. TI        | ME          | TO          |              | ATION  | RE           | AC   | HES      | <u> </u>                                | <i>38</i> | 0.   | 9.            |          |              |  |                |
|          | 2. TI        | ME          | TO          |              | ATION  | RE           | AC   | HES      | <u> </u>                                | <i>38</i> | 0.   | 9.            |          |              |  |                |
|          | 2. TI        | ME          | TO          |              | ATION  | RE           | AC   | HES      | <u> </u>                                | <i>38</i> | HE   | 9.            |          |              |  |                |
|          | 2. TI        | ME          | TO          |              | ATION  | RE           | AC   | HES      | <u> </u>                                | <i>38</i> | HE   | 9.            | 30.5     |              |  |                |
|          | 2. TI        | ME          | TO          |              | ATION  | RE           | AC   | HES      | <u> </u>                                | <i>38</i> | HE   | 9.            |          |              |  |                |
|          | 2. TI        | ME          | TO          |              | ATION  | RE           | AC   | HES      | <u> </u>                                | <i>38</i> | HE   | 9.            |          |              |  |                |
|          | 2. TI        | ME          | TO          |              | ATION  | RE           | AC   | HES      | <u> </u>                                | <i>38</i> | HE<br>EL   | 9.            |          | 2            | 74.4   |                |
|          | 2. TI        | ME          | TO          | DEVI         | ELOP   | BRI          | AC   | HES      | <u> </u>                                | <i>38</i> | HE<br>EL   | 9.            | 30.9     | 2            | 74.4   |                |
|          | 2. TI        | ME          | TO          | DEVI         | ATION  | BRI          | AC   | HES      | <u> </u>                                | <i>38</i> | HE<br>EL   | 9.            | 30.9     | 2            | 74.4   |                |
|          | 2. TI        | ME<br>ECTI  | ON          | DEVI         | ELOP   | BRI          | EAL  | HE:      |   | 38        | HE<br>EL   | 9.            | 30.9     | 2            | 74.4   |                |



| CH ENGINEERS $T_n L_{=}$    | RUALE LAKE  | Dam                                    |                                       | pet  |
|-----------------------------|-------------|--|---------------------------------------|--|
| ct                          | KUMIC DAKE  | <u> </u>                               |                                       | Date <u>2-25-81</u><br>Date <u>2/27/81</u> |
|                             |             |  |                                       |  |
|                             | Closs SEC   | TION                                   | : '                                   |  |
|                             | END OF R    | EACH 1                                 |                                       |  |
|                             |             | :                                      |                                       |  |
|                             | S= 0.0063   | L = 30                                 | 0 [F+]                                | _  |
|                             |             |  |                                       |  |
| ert 0                       |             |  |                                       |  |
| STA. 0<br>  EL. 380.0       |             |  |                                       | STA-1015                                   |
|                             |             | <del></del>                            | /2                                    | L.380.0                                    |
|                             |             | <del> </del>                           |                                       |  |
|                             |             |  |                                       | į  |
| 5TA. 300                    |             |  | STA. 7                                |  |
| EL. 379.5                   |             |  | EL. 378                               | 3.7  |
|                             |             | STA                                    | . 523                                 | <del></del>                                |
| 57A.500                     |             | EL.                                    | 377.8                                 | - <del></del>                              |
| L.319.7<br>3TA.510          |             | STA.                                   | KIE                                   | ·  |
| EL. 371.5                   |             | EL. 37                                 |                                       | · · · · · · · · · · · · · · · · · · ·      |
|                             |             |  |                                       |  |
|                             |             | ······································ |                                       | - <u> </u>                                 |
| C                           | ROSS SECTIO | N                                      |                                       |  |
| EN                          | D OF REAC   | H 2.                                   | ·                                     |  |
|                             |             |  | · · · · · · · · · · · · · · · · · · · |  |
| <u> </u>                    | 0.006       | = 1,900                                | [F+]                                  |  |
|                             |             |  |                                       |  |
| CTA O                       |             |  | STA, 425                              |  |
| STA. 0<br>EL. 367.0         |             | • •                                    | EL. 367.0                             | \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \      |
| y                           |             |  |                                       | min o o o o o o o o o o o o o o o o o o o  |
|                             |             | 1                                      |                                       |  |
|                             |             |  |                                       |  |
| STA. 100                    |             |  | STA 375                               |  |
| 366'0 STA. 200              | ' '         | STA. 22                                | 5 FL 366.0                            |  |
| 366.0 STA. 200<br>EL. 365.0 | · ·         | STA. 22<br>EL. 365.<br>STA. 216        | 5 FL 366.0                            |  |

HEC - 1 - DAM PRINTOUT

Overtopping Analysis

| 1   | N   | ATTONAL   | DAM SAFET   | Y FROGR  | AH -                    |                             | <del></del>                                 |              |       |       |
|---|---|---|---|--|-------------------------|-----------------------------|---|--------------|-------|-------|
| 12  |   |   | RVALE DAP   |  |                         |                             |   |              |       |       |
| A3  |   |   | R STORM F   |  |                         |                             |   |              |       |       |
| B   | 300   | 0   | 15  |  |                         |                             | 0   | 0            | 4     |       |
| B1  | 5   |   |   |  |                         |                             | _   | _            | -     |       |
| J   | 1   | 1   | 1   |  |                         |                             |   |              |       |       |
| IJŢ   |   | · <u>-</u>  |   |  |                         |                             | ·   |              |       |       |
| K   | 0   | LAKE  |   | •  | 0                       | 0                           | 1   |              |       |       |
| K1  | 11  | NFLOW HY  | DROGRAPH  | TO LAKE  | INTERVAL                | E DAM                       | •   |              |       |       |
| H   | 0   | 2   | 0.53  |  | 0.53                    | 7                           |   |              | 1     |       |
| 0   | 96  |   |   |  |                         |                             | ,   | •            |       |       |
| 01  | 0.019   | 0.019   | 0.019   | 0.019  | 0.019                   | 0.019                       | 0.019                                       | 0.019        | 0.019 | 0.019 |
| 01  | 0.019   | 0.019   | 0.019   | 0.019  | 0.019                   | 0.019                       | 0.019                                       | 0.019        | 0.019 | 0.019 |
|   | 0.019   | 0.019   | 0.019   | 0.019  | 0.019                   | 0.019                       | 0.019                                       | 0.019        | 0.019 | 0.019 |
|   | 0.019   | 0.019   | 0.019   | 0.019  | 0.019                   | 0.019                       | 0.019                                       | 0.019        | 0.019 | 0.019 |
|   | 0.019   | 0.019   | 0.019   | 0.019  | 0.019                   | 0.019                       | 0.019                                       | 0.019        | 0.038 | 0.038 |
|   | 0.038   | 0.03B   | 0.038   | 0.038  | 0.038                   | 0.038                       | 0.038                                       | 0.038        | 0.038 | 0.038 |
|   | 0.083   | 0.083   | 0.083   | 0.083  | 0.163                   | 0.163                       | 0.163                                       | 0.163        | 0.750 | 0.750 |
|   | 0.750   | 0.750   | 0.183   | 0.163  | 0.163                   | 0.163                       | 0.083                                       | 0.083        | 0.083 | 0.0B3 |
|   | 0.083   | 0.083   | 0.083   | 0.083  | 0.038                   | 0.03B                       | 0.038                                       | 0.038        | 9.038 | 0.038 |
|   | 0.038   | 0.038   | 0.038   | 0.038  | 0.038                   | 0.038                       | <del></del>                                 | A - 1 = -    |       |       |
| T   |   |   |   |  |                         |                             | 1.5   | 0.15         |       |       |
| W2  |   | 0.78  |   | •  | •                       |                             |   |              |       |       |
| <del>X</del> -  | -1.0  | -0.05<br>DAM  | 2.0   |  |                         |                             |   |              |       |       |
| K1  | _   |   | CHARGE TI   | JEOUGH B   | AW                      |                             |   |              |       |       |
| Y.  | ~   | DOIE DIS  | CHARGE II   | ע הטטטאר<br>1  | nn<br>1                 |                             |   |              |       |       |
| -   |   |   |   | _  | •                       |                             |   |              |       |       |
| V 1   | •   |   |   |  |                         |                             | -378.7                                      |              |       |       |
| Y1  | 1<br>379.7  | = 379   | = 379.5   | 380  | 380.9                   | 382                         | -378.7<br>383                               | -1<br>384    |       |       |
| Y4  | 378.7   | ≈ 379 <sup>3</sup>  | 379.5   | 380  | 380.9                   | 382                         | 383   | 384          |       |       |
| Y4<br>Y5  | 378.7<br>0<br>0   | = 379 = 3.3   | 14.3  | 29.6   | 380.9                   | 382<br>94.3                 |   | _            |       |       |
| Y4<br>Y5  | 378.7 °<br>0<br>0   | 379 3.3<br>35.8   | 14.3  |  |                         |                             | 383   | 384          |       |       |
| Y4<br>Y5<br>\$S<br>\$E  | 378.7 ·   | = 379 = 3.3   | 14.3  | 29.6   |                         |                             | 383   | 384          |       |       |
| Y4<br>Y5<br>\$S<br>\$E<br>\$\$  | 378.7<br>0<br>0<br>374.4  | 379 3.3<br>35.8   | 14.3  | 29.6   |                         |                             | 383   | 384          |       |       |
| Y4<br>Y5<br>\$S<br>\$E<br>\$\$  | 378.7<br>0<br>0<br>374.4<br>378.7<br>380.9                              | 379 3<br>3.3<br>35.8<br>378   | 14.3<br>. 64.2<br>380   | 29.6<br>614.2<br>400   | 66.6                    |                             | 383   | 384          |       |       |
| Y4<br>Y5<br>\$5<br>\$E<br>\$5   | 378.7<br>0<br>0<br>374.4<br>378.7<br>380.9                              | 379 3<br>3.3<br>35.8<br>378   | 14.3<br>. 64.2<br>380   | 29.6<br>614.2<br>400   | 66.6                    |                             | 383<br>113.7                                | 384          |       |       |
| Y4<br>Y5<br>\$5<br>\$E<br>\$\$<br>\$!   | 378.7<br>0<br>0<br>374.4<br>378.7<br>380.9                              | 379 3<br>3.3<br>35.8<br>378   | 14.3<br>. 64.2<br>380   | 29.6<br>614.2<br>400   | 66.6                    |                             | 383<br>113.7                                | 384          |       |       |
| Y4<br>Y5<br>\$S<br>\$E<br>\$\$<br>\$II<br>K   | 378.7<br>0<br>0<br>374.4<br>378.7<br>380.9                              | 379 3<br>3.3<br>35.8<br>378   | 14.3<br>. 64.2<br>380   | 29.6<br>614.2<br>400<br>120  | 66.6                    |                             | 383<br>113.7                                | 384          |       |       |
| Y4<br>Y5<br>\$S<br>\$E<br>\$\$<br>\$U<br>K<br>K1<br>Y   | 378.7<br>0<br>0<br>374.4<br>378.7<br>380.9<br>1<br>C                    | 379 3<br>3.3<br>35.8<br>378   | 14.3<br>. 64.2<br>380   | 29.6<br>614.2<br>400<br>120  | 66.6                    |                             | 383<br>113.7                                | 384          |       |       |
| Y4<br>Y5<br>\$S<br>\$E<br>\$\$<br>\$K<br>K1<br>Y1<br>Y6<br>Y7                                     | 378.7<br>0<br>0<br>374.4<br>378.7<br>380.9<br>1<br>C                    | 379 3.3 35.8 378 2.63 1 HANNEL R 0.035 380  | 14.3<br>. 64.2<br>380<br>1.5<br>OUTING R                                | 29.6<br>614.2<br>400<br>120<br>EACH 1 1<br>371.5<br>379.5                        | 1                       | 94.3                        | 383<br>113.7                                | 384          | 515   | 371.5 |
| Y4<br>Y5<br>\$S<br>\$E<br>\$\$<br>K<br>K1<br>Y1<br>Y1<br>Y7<br>Y7                                 | 378.7<br>0<br>0<br>374.4<br>378.7<br>380.9<br>1<br>C                    | 379 3.3<br>35.8<br>378<br>2.63<br>1<br>HANNEL R   | 14.3<br>. 64.2<br>380<br>1.5<br>OUTING R                                | 29.6<br>614.2<br>400<br>120<br>EACH 1-1<br>1                                     | 1 380                   | 94.3                        | 383<br>113.7<br>1<br>                       | 394<br>130.3 | 515   | 371.5 |
| Y4<br>Y5<br>\$S<br>\$E<br>\$\$<br>K<br>K1<br>Y1<br>Y1<br>Y7<br>K                                  | 378.7<br>0<br>0<br>374.4<br>378.7<br>380.9<br>1<br>C                    | 379 3.3<br>35.8<br>378<br>2.63<br>1<br>HANNEL R<br>0.035<br>380<br>377.8<br>2               | 14.3<br>.64.2<br>380<br>1.5<br>OUTING R                                 | 29.6<br>614.2<br>400<br>120<br>EACH 1<br>1<br>371.5<br>379.5<br>378.7            | 1<br>380<br>500<br>1015 | 300<br>379.2                | 383<br>113.7<br>1<br>                       | 394<br>130.3 | 515   | 371.5 |
| Y4<br>Y5<br>\$S<br>\$E<br>\$\$<br>K<br>K1<br>Y1<br>Y1<br>Y7<br>K1                                 | 378.7<br>0<br>0<br>374.4<br>378.7<br>380.9<br>1<br>C                    | 379 3.3<br>35.8<br>378<br>2.63<br>1<br>HANNEL R<br>0.035<br>380<br>377.8<br>2               | 14.3<br>. 64.2<br>380<br>1.5<br>OUTING R                                | 29.6<br>614.2<br>400<br>120<br>EACH 1<br>1<br>371.5<br>379.5<br>378.7<br>REACH 2 | 1<br>380<br>500<br>1015 | 300<br>379.2                | 383<br>113.7<br>1<br><br>0.0063<br>510      | 394<br>130.3 | 515   | 371.5 |
| Y4<br>Y5<br>\$S<br>\$E<br>\$\$<br>K1<br>Y1<br>Y1<br>Y7<br>K1<br>Y7<br>K1                          | 378.7<br>0<br>0<br>374.4<br>378.7<br>380.9<br>1<br>C                    | 379 3.3<br>35.8<br>378<br>2.63<br>1<br>HANNEL R<br>0.035<br>380<br>377.8<br>2               | 14.3<br>.64.2<br>380<br>1.5<br>OUTING R                                 | 29.6<br>614.2<br>400<br>120<br>EACH 1<br>1<br>371.5<br>379.5<br>378.7            | 1<br>380<br>500<br>1015 | 300<br>379.2                | 383<br>113.7<br>1<br><br>0.0063<br>510      | 394<br>130.3 | 515   | 371.5 |
| Y4<br>Y5<br>\$\$<br>\$E<br>\$\$<br>\$E<br>\$\$<br>K<br>K1<br>Y Y1<br>Y7<br>K<br>K1<br>Y Y7<br>K   | 378.7<br>0<br>0<br>374.4<br>378.7<br>380.9<br>1<br>C                    | 379<br>3.3<br>35.8<br>378<br>2.63<br>1<br>HANNEL R<br>0.035<br>380<br>377.8<br>2<br>CHANNEL | 14.3<br>64.2<br>380<br>1.5<br>OUTING R<br>0.1<br>300<br>723             | 29.6<br>614.2<br>400<br>120<br>EACH 1<br>371.5<br>379.5<br>378.7<br>REACH 2      | 1<br>380<br>500<br>1015 | 94.3<br>300<br>379.2<br>380 | 383<br>113.7<br>1<br>0.0063<br>510          | 394<br>130.3 | 515   | 371.5 |
| Y44<br>Y55<br>\$\$<br>\$E<br>\$\$<br>\$\$<br>K1<br>Y11<br>Y6<br>Y77<br>K1<br>Y11<br>Y6            | 378.7<br>0<br>374.4<br>378.7<br>380.9<br>1<br>0.1<br>0.523<br>1         | 379 3.3<br>35.8<br>378 2.63<br>1 HANNEL R<br>0.035 380 377.8<br>2 CHANNEL                   | 14.3<br>.64.2<br>380<br>1.5<br>OUTING R<br>0.1<br>300<br>723<br>ROUTING | 29.6<br>614.2<br>400<br>120<br>EACH 1<br>371.5<br>379.5<br>378.7<br>REACH 2      | 1<br>380<br>500<br>1015 | 300<br>379.2<br>380         | 383<br>113.7<br>1<br><br>0.0063<br>510<br>1 | 394<br>130.3 |       |       |
| Y44<br>Y55<br>\$\$<br>\$E<br>\$\$<br>\$\$<br>K1<br>Y146<br>Y77<br>K1<br>Y76<br>Y77<br>K1<br>Y77   | 378.7<br>0<br>374.4<br>378.7<br>380.7<br>1<br>0.1<br>0<br>523<br>1      | 379 3.3 35.8 378 2.63 1 HANNEL R 0.035 380 377.8 2 CHANNEL                                  | 14.3<br>.64.2<br>380<br>1.5<br>OUTING R<br>0.1<br>300<br>723<br>ROUTING | 29.6<br>614.2<br>400<br>120<br>EACH 1<br>1<br>371.5<br>379.5<br>378.7<br>REACH 2 | 1<br>380<br>500<br>1015 | 300<br>379.2<br>380         | 383<br>113.7<br>1<br>0.0063<br>510          | 394<br>130.3 | 515   | 371.5 |
| Y4<br>Y5<br>\$S<br>\$E<br>\$\$<br>\$K<br>K1<br>Y17<br>Y7<br>K1<br>Y7<br>Y7<br>Y7<br>Y7            | 378.7<br>0<br>0<br>374.4<br>378.7<br>380.9<br>1<br>0.1<br>0<br>523<br>1 | 379 3.3<br>35.8<br>378 2.63<br>1 HANNEL R<br>0.035 380 377.8<br>2 CHANNEL                   | 14.3<br>.64.2<br>380<br>1.5<br>OUTING R<br>0.1<br>300<br>723<br>ROUTING | 29.6<br>614.2<br>400<br>120<br>EACH 1<br>371.5<br>379.5<br>378.7<br>REACH 2      | 1<br>380<br>500<br>1015 | 300<br>379.2<br>380         | 383<br>113.7<br>1<br><br>0.0063<br>510<br>1 | 394<br>130.3 |       |       |
| Y4<br>Y5<br>\$S<br>\$E<br>\$\$<br>\$K<br>K1<br>Y1<br>Y7<br>K1<br>Y7<br>K1<br>Y7<br>K1<br>Y7<br>K1 | 378.7<br>0<br>374.4<br>378.7<br>380.7<br>1<br>0.1<br>0<br>523<br>1      | 379 3.3 35.8 378 2.63 1 HANNEL R 0.035 380 377.8 2 CHANNEL                                  | 14.3<br>.64.2<br>380<br>1.5<br>OUTING R<br>0.1<br>300<br>723<br>ROUTING | 29.6<br>614.2<br>400<br>120<br>EACH 1<br>1<br>371.5<br>379.5<br>378.7<br>REACH 2 | 1<br>380<br>500<br>1015 | 300<br>379.2<br>380         | 383<br>113.7<br>1<br><br>0.0063<br>510<br>1 | 394<br>130.3 |       |       |
| Y4<br>Y5<br>\$S<br>\$E<br>\$\$<br>\$K<br>K1<br>Y17<br>Y7<br>K1<br>Y7<br>Y7<br>Y7<br>Y7            | 378.7<br>0<br>0<br>374.4<br>378.7<br>380.9<br>1<br>0.1<br>0<br>523<br>1 | 379 3.3 35.8 378 2.63 1 HANNEL R 0.035 380 377.8 2 CHANNEL                                  | 14.3<br>.64.2<br>380<br>1.5<br>OUTING R<br>0.1<br>300<br>723<br>ROUTING | 29.6<br>614.2<br>400<br>120<br>EACH 1<br>1<br>371.5<br>379.5<br>378.7<br>REACH 2 | 1<br>380<br>500<br>1015 | 300<br>379.2<br>380         | 383<br>113.7<br>1<br><br>0.0063<br>510<br>1 | 394<br>130.3 |       |       |

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| ****                | ****                        | #<br>#<br># | ****               | *******                      |             | ********       | ***            | **           | ******** |
|---------------------|-----------------------------|-------------|--------------------|------------------------------|-------------|----------------|----------------|--------------|----------|
|                     |                             |             | HYDROGRAFH ROUTING | H ROUTE                      | NG          |                | 1              |              |          |
|                     | ROUTE DISCHARGE THROUGH DAM | THROUGH I   | AM                 |                              |             |                |                |              |          |
|                     | ISTAG                       | ICOMP<br>1  |                    | ITAPE<br>0                   | JPLT        | JFRT           | INAME          | ISTAGE       | IAUTO    |
|                     | 0.0 0.000                   | AVG<br>0.00 | ROUTI<br>IRES 1    | ISAME                        | IOFT<br>0   | IFHF           |                | LS7R<br>0    |          |
|                     | NBTPS                       | NSTDL<br>0  | LAG                | AMSKK<br>0.000               | × 000.0     | 1SK<br>0.000   | STORA<br>-379. | ISPRAT<br>-1 | -        |
| STAGE 378 °C        | 379.00 37                   | 379.50      | 380.00             | 380                          | 380.90      | 382.00         |                | 383.00       | 384.00   |
| FLOW 0.0.           | 3.30                        | 14.30       | 29.60              | 99                           | 99.99       | 94.30          |                | 113.70       | 130,30   |
| CAPACITY®           | 36.                         | 64.         | 614.               |                              |             |                |                |              |          |
| ELEVATION           | . 378.                      | 380.        | 400.               |                              | •           |                |                |              |          |
|                     | CREL SPUID<br>378.7 0.0     |             | 0.0 0.0            | TELEUL<br>0.0                |             | COUL CAREA     |                | EXFL<br>0.0  |          |
|                     |                             |             | TOPEL<br>380.9     | 0AH DATA<br>COOD EX<br>2.6 1 | EXFD<br>1.5 | DAMUID<br>120. |                |              |          |
| FEAK DUTFLOW 18 369 | 369. AT TIME 19.25 HOURS    | HOURS       |                    |                              |             |                |                |              |          |

| STATIO   1   1   1   1   1   1   1   1   1   |            |         |      |                     | =                | RATI               | RATIOS APPLIED TO FLOWS | O FLOWS              |                     |                    |
|--|------------|---------|------|---------------------|------------------|--------------------|-------------------------|----------------------|---------------------|--------------------|
| ТОТЕВ ТО ТОТЕ 1.37) ( 20.19) ( 20.19) ( 20.10) ( 20.10) ( 20.10) ( 20.10) ( 20.10) ( 20.10) ( 20.10) ( 20.10) ( 20.10) ( 20.10) ( 20.40) ( 20.10) ( 20.40) ( 20.10) ( 20.40) ( 20.10) ( 20.40) ( 20.10) ( 20.40) ( 20.10) ( 20.40) ( 20.10) ( 20.40) ( 20.10) ( 20.40) ( 20.10) | DFERATION" | STATION | AREA |                     | 10               |                    |                         |                      |                     |                    |
| FLAN 1   | HYDERAPH   |         | .53  | -                   | 713.             |                    |                         |                      |                     |                    |
| 1.53   1.350   | KOUTED TO  | DAM     | 1.37 | -                   | _                |                    |                         |                      |                     |                    |
| SUNHARY OF DAM SAFETY ANALYSIS   | ROUTEB TO  | 1       |      | -                   | 370.             |                    |                         | -                    |                     |                    |
| 1  | ROUTED TO  | 8       | .53  | 1,                  | 367.<br>10.38)(  | •                  |                         |                      |                     |                    |
| The continue of the continue |            |         |      |                     | ัง               |                    | SAFETY                  | .YSIS                |                     |                    |
| SIURAUE 40. 0. 67.  OUTFLOW 001FLOW 001FLOW DURATION TIME OF MAXIMUM MAXIMUM DURATION TIME OF HOURS  W.S.ELEV UVER UAN AC-FT CFS HOURS HOURS  381.82 .92 114. 369. 5.00 19.25  PLAN 1 STATION 1  PLAN 1 STATION 2  PLAN 1 STATION 2  PLAN 1 STATION 2  PLAN 1 STATION 71HE  RATIO FLOW.CFS STAGE.FT HOURS  1.00 370. 376.5 19.25  1.00 357. 364.4 19.25  | PLAN       | ) )     |      | ELEVATION           | INITIA           | VALUE              |                         | - 106                | 0F DAN<br>380.90    |                    |
| RESERVOIR DEPTH STORAGE OUTFLOW DURATION TIHE OF MAX OUTFLOW GVER TOP MAX OUTFLOW TIME RATIO FLOW, CFS STAGE, FT HOURS TO BLAN 1 STATION 2  RATIO FLOW, CFS STAGE, FT HOURS FLAN 1 STATION 2  RATIO FLOW, CFS STAGE, FT HOURS TO BLAN 1 STATION 2  1.00 370, 376.5 19.25  |            |         |      | STUKAGE             |                  | • •                | Ö                       |                      | 67.                 |                    |
| # 5.5 ELEV OVER DAM AC-FI CFS HOURS HOURS  381.82 .92 114. 369. 5.00 19.25  RATIO HAXIMUM MAXIMUM TIME  RATIO FLOW, CFS STAGE, FT HOURS  1.00 370. 376.5 19.25  FLAN 1 STATION 2  RATIO FLOW, CFS STAGE, FT HOURS  1.00 357. 364.4 19.25   |            | RA      |      | HAXIMUM<br>ESERVOIR | MAXIMUM<br>DEPTH | MAXIMUM<br>STORAGE | MAXIMUM<br>OUTFLOW      | DURATION<br>DVER TOP | TIME OF MAX DUTFLOW | TIME OF<br>FAILURE |
| 381.82 .92 114. 369. 5.00 19.25  PLAN 1 STATION 1  RATIO FLOW, CFS STAGE, FT HOURS  1.00 370. 376.5 19.25  PLAN 1 STATION 2  RATIO FLOW, CFS STAGE, FT HOURS  RATIO FLOW, CFS STAGE, FT HOURS  1.00 370. 354.4 19.25   |            |         |      | W.S.ELEV            | OVER DAM         | AC-F1              | s<br>D                  | 400%                 | ROOM                | 6400               |
| STATION   1  |            | 1:      | 00   | 381.82              | .92              | 114.               | 369.                    | 2.00                 | 19.25               | 0.00               |
| HAXIMUM MAXIMUM TIME FLOW,CFS STAGE,FT HOURS 370, 376.5 19.25  **LAN 1 STATION 2 HAXIMUM HAXIMUM TIME FLOW,CFS STAGE,FT HOURS 367. 364.4 19.25   |            |         |      |                     |                  | - 1                | STATION                 | 7                    |                     | ;                  |
| 370. 376.5 19.25  PLAN 1 STATION 2  HAXIHUM HAXIMUM TIME FLOW.CFB 8TAGE.FT HOURS 367. 364.4 19.25  |            |         |      |                     | RATIO            | F                  | MAXINUM<br>STAGE,FT     |                      |                     |                    |
| PLAN 1 STATION 2 HAXIHUM HAXIHUM TIME FLOW,CFS STAGE,FT HOURS 367, 364,4 19.25   |            |         |      |                     | 1.00             |                    | 376.5                   |                      |                     |                    |
| HAXIHUH HAXIHUH TIHE<br>FLOW.CFS STAGE.FT HOURS<br>367. 364.4 19.25  |            |         |      |                     |                  |                    | STATION                 | 7                    |                     |                    |
| 367. 364.4 19.25   |            |         |      |                     | RATIO            |                    | HAXIHUH<br>BIAGE,FI     | TIME                 |                     |                    |
|  |            |         |      |                     | 1.00             |                    |                         | 19.25                |                     |                    |

HEC - 1 - DAM PRINTOUT

Breach Analysis

| 1 <u>3</u><br>15 |                  | KE INTER     | א אמנוב    |                |             |              |             |             |                                       |                                       |
|------------------|------------------|--------------|------------|----------------|-------------|--------------|-------------|-------------|---------------------------------------|---------------------------------------|
| 13               | 300              | 100 1246     | 15         | 001110         |             |              | 0           | 0.          | 4                                     |                                       |
| 31               | 5                | •            |            |                |             |              | •           |             |                                       |                                       |
| <del>;</del>     | <del>- i</del> - | 1            | 1          |                |             |              |             |             | <del></del>                           |                                       |
| 11               | i                | •            | •          |                |             |              |             |             |                                       |                                       |
| ζ-               | ō                | LAKE         |            |                | 0           | 0            | 1           |             |                                       |                                       |
| 1                | I                | NELOW HYI    | ROGRAPH    | TO LAKE        | INTERVAL    | E TIAH       |             |             |                                       |                                       |
| 1                | 0                | 2            | 0.53       |                | 0.53        | 0            |             |             | 1                                     |                                       |
| 3                | 96               |              |            |                |             | •            |             |             |                                       |                                       |
| )1               | 0.019            | 0.019        | 0.019      | 0.019          | 0.019       | 0.019        | 0.019       | 0.019       | 0.019                                 | 0.019                                 |
| 1                | 0.019            | 0.019        | 0.019      | 0.019          | 0.019       | 0.019        | 0.019       | 0.019       | 0.019                                 | 0.019                                 |
| 1                | 0.019            | 0.019        | 0.019      | 0.019          | 0.019       | 0.019        | 0.019       | 0.019       | 0.019                                 | 0.019                                 |
|                  | 0.019            | 0.019        | 0.019      | 0.019          | 0.019       | 0.019        | 0.019       | 0.019       | 0.019                                 |                                       |
|                  | 0.019            | 0.019        | 0.019      | 0.019          | 0.019       | 0.019        | 0.019       | 0.019       | 0.038                                 | 0.038                                 |
|                  | 0.038            | 0.038        | 0.038      | 0.038          | 0.038       | 0.038        | 0.038       | 0.038       | 0.038                                 | 0.038                                 |
|                  | 0.083            | 0.083        | 0.083      | 0.083          | 0.163       | 0.163        | 0.163       | 0.163       | 0.750                                 | 0.750                                 |
|                  | 0.750            | 0.750        | 0.163      | 0.163          | 0.163       | 0.163        | 0.083       | 0.083       | 0.083                                 | 0.083                                 |
|                  | 0.083            | 0.083        | 0.083      | 0.083          | 0.038       | 0.038        | 0.038       | 0.038       | 0.038                                 | 0.038                                 |
|                  | 0.038            | 0.038        | 0.038      | 0.038          | 0.038       | 0.038        | 1.5         | 0.15        |                                       |                                       |
| 1                |                  |              |            |                | . •         |              | 1.5         | 0.15        |                                       |                                       |
| M2               | -1.0             | -0.05        | 2.0        | ····           | <del></del> |              | <del></del> | <del></del> | <u> </u>                              |                                       |
| A<br>K           | 1                | DAM          | 2.0        |                |             |              |             |             |                                       |                                       |
| K1               | _                | OUTE DISC    | THARGE TH  | an Hallos      | м           |              |             |             |                                       |                                       |
| Ŷ                |                  | 00.2 213     | JIHNOL II  | 1.             | 1           | <del></del>  | <del></del> |             |                                       |                                       |
| Ý1               | 1                |              |            | •              | . •         |              | -378.7      | -1          |                                       |                                       |
|                  | 378.7            | 379          | 379.5      | 380            | 380.9       | 382          | 383         | 384         |                                       |                                       |
|                  | - 40             | 3,73         | 14.3       | 29.6           | 66.6        | 94.3         | 113.7       | 130.3       |                                       | · · · · · · · · · · · · · · · · · · · |
| \$ 5             | Ö                | 35.8         | 64.2       | 614.2          |             |              |             |             |                                       |                                       |
| \$E              | 374.4            | 378          | 380        | 400            |             |              |             |             |                                       |                                       |
|                  | 378.7            |              |            |                |             |              |             |             |                                       |                                       |
|                  | 380.9            | 2.63         | 1.5        | 120            |             |              |             |             |                                       |                                       |
| \$ B             | 25               | 1_           | 374.4      | 1.0            | 378_        | 380.9        |             |             | · · · · · · · · · · · · · · · · · · · |                                       |
| K                |                  | 1            |            |                |             |              | 1           |             |                                       |                                       |
| K1               | С                | HANNEL R     | וא טאנדטט  |                | _           |              |             |             |                                       |                                       |
| Y                |                  |              | .•         |                |             |              |             |             |                                       |                                       |
| Y1               | 1                |              |            | 774 5          | ~~~         | 744          | 0.0013      |             |                                       |                                       |
| 4 6              | 0.1              | 0.035        | 0.1        | 371.5          | 380         | 300          | 0.0063      | 774 =       | 515                                   | 371.5                                 |
| Y7<br>Y7         | 0<br>523         | 380<br>377.8 | 300<br>723 | 379.5<br>378.7 | 500<br>1015 | 379.2<br>380 | 510         | 371.5       | 515                                   | 3/1.5                                 |
|                  | 523              | 3//.8        | 123        | 3/0./          | 1015        | 200          | 1           |             |                                       |                                       |
| K<br>K1          | . 1              | CUANNE       | ROUTING    | BEACH 3        |             |              | 1           |             |                                       |                                       |
| <u> </u>         |                  | CHHNNEL      | KOOIING    | 1              | 1           |              |             |             |                                       | <del></del>                           |
| Y1               | 1                |              |            | . •            | •           |              |             |             |                                       |                                       |
| Y 6              | 0.1              | 0.035        | 0.1        | 360            | 367         | 1900         | 0.006       | •           |                                       |                                       |
| <del>77</del>    | - 0.1            | 367          | • 100      | 366            | 200         | 365          | 210         | 360         | 215                                   | 360                                   |
| Ý7               | 225              | 365          | 325        | 366            | 425         | 367          |             |             |                                       |                                       |
| ĸ                | 99               |              |            |                |             |              |             |             |                                       |                                       |

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| 15TAG 1CUMP 1 15TAG 1CUMP 1 15TAG 1CUMP 1 1 0 0.00 14.30 0 14.30 0 14.30 36. 64. 78. 380. 78. 59110 COG 8.7 0.0 0.0 8.7 0.0 0.0 8.7 0.0 0.0 8.7 0.0 0.0 | HYDROGRAPH ROUTING                  | ON ITAPE JPLI JPRI INAME ISTAGE IAUTO | AMSKK X TSK BIOKA ISPKA<br>0.000 0.000 0.000 -379 | 60 66.60 94.30 113.70 130.30 |     | EXPW ELEUL COOL CAREA EXPL | DAM DATA<br>COOR EXPL DAMUID<br>2.6 1.5 120. | DAH BREACH DATA<br>ELBH TFAIL WSEL FAILEL<br>374.40 1.00 378.00 380.90 |                                  |
|---|-------------------------------------|---|---|------------------------------|-----|----------------------------|--|--|----------------------------------|
| EDUTE DISC<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1   | **********  HYDRO HARGE THROUGH DAM | LUONF IEC   | NSTDL<br>0<br>579.50                              |                              | 64. | 380. 400.<br>SPWID COOM    | 10FEL  |  |                                  |
|   |                                     |   | 00.478  |                              | • 0 | 374.                       |  |  | BEGIN DAM FAILURE AT 18.50 HOURS |

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| STATION | AREA PI                                       | PLAN                            | 1.00 ll                      | KAI                         | RATIOS APPLIED TO FLOWS         | TO FLOWS                      |                                 |                       |
|---------|---|---------------------------------|------------------------------|-----------------------------|---------------------------------|-------------------------------|---------------------------------|-----------------------|
|         | .53   | -   -                           | 1340.                        |                             |                                 |                               | -                               |                       |
|         | 1,37)   | -                               | 36.49)(                      |                             |                                 |                               |                                 |                       |
|         | 1,37)   | ,~                              | -                            |                             |                                 |                               |                                 |                       |
|         |   |                                 | <b>93</b>                    | MMARY OF DA.                | SUMMAKY OF DAM SAFETY ANALYSIS  | .kere                         |                                 |                       |
|         | ELEVATIO<br>STORAGE<br>DUTFLOW                | ELEVATION<br>STORAGE<br>DUTFLOW | 378<br>378                   |                             | SPILLWAY CREST<br>378.70<br>46. | 101                           | UF UAN<br>380.90<br>89.         |                       |
| E 8 #   | RATID HAXIMUM<br>OF RESERVOIR<br>PHF W.S.ELEV | UH<br>OIR<br>Lev                | HAXIHUH<br>DEPTH<br>OVER DAN | HAXIHUM<br>STORAGE<br>AC-FI | HAXTHUH<br>OUTFLOW<br>CFS       | DURATION<br>OVER TOP<br>HOURS | TIRE OF<br>MAX QUIFLOW<br>HOURS | TIME OF FAILURE HOURS |
| 1.00    | 381.35  | 35                              | .45                          | 101.                        | 1340.                           | 1.00                          | 19.50                           | 18.50                 |
|         | •   |                                 | ā.                           | FLAN 1                      | STATION                         | 1 .                           |                                 |                       |
|         |   |                                 | RATIO                        | HAXIHUM<br>FLOW, CFS        | HAXIHUM<br>STAGE,FT             | TIME<br>HOURS                 |                                 |                       |
|         |   |                                 | 1.00                         | 1288.                       | 379.3                           | 19.50                         |                                 | ,                     |
|         |   |                                 |                              | FLAN 1                      | STATION                         | 7                             |                                 |                       |
|         |   |                                 | RATIO                        | MAXIMUM<br>FLOW,CFS         | MAXIHUM<br>STAGE,FT             | TIME                          | ·                               |                       |
|         |   | •                               | 1.00                         | 1136.                       | 366.4                           | 19.75                         |                                 | !                     |

APPENDIX 5

Bibliography

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